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COMPUTER PROGRAMS FOR ESTIMATING AIRCRAFT
TAKEOFF AND LANDING PERFORMANCE

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ABSTRACT

A set of computer programs has been developed to estimate the takeoff and landing maneuver of a given aircraft. The program is applicable to conventional, vectored lift and powered-lift concept aircraft. Portions of the program may also be used to evaluate the static performance of these types of aircraft. The aircraft is treated as a point mass confined to motion in a vertical plane, and rotational dynamics have been neglected. The required input is described and a sample case is presented.

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INTRODUCTION

A set of computer programs has been developed to estimate the takeoff and landing maneuver of a given aircraft. The program is applicable to conventional, vectored lift and powered-lift concept aircraft. Portions of the program may also be used to evaluate the static performance of these type aircraft. The aircraft is treated as a point mass confined to motion in a vertical plane, and the rotational dynamics have been neglected. The takeoff subroutines are a modification and simplification of an unpublished program by V. R. Corsiglia of Ames Research Center.

The user is required to provide two subroutines which compute the total force coefficients along and normal to the flight path, and determine various required engine characteristics.

This report describes the various subroutines and the required input, the equations used, and the computational techniques involved. Also included is a listing of the total program and an example case.

NOTATION

Symbol	Fortran Name	
a_n	S(9)	- acceleration normal to flight path (rad/sec ²)
a_t	T(6), S(8)	- acceleration along flight path (ft/sec ²)
C_x	CX	- force coefficient along flight path
C_y	CY	- force coefficient normal to flight path
ENP	ENP	- number of engines
g		- acceleration due to gravity (ft/sec ²)
h	HABS, S(7)	- absolute altitude (ft)
i_w	EYEW, EYEWNG	- incidence of wing (deg)
LF	XLF	- load factor
q		- dynamic pressure (lb/ft ²)
R/C	S(11), ROC, RTCL	- rate of climb (ft/sec, fpm)
S	SW, SWING	- reference wing area (ft ²)
T	THRUST	- thrust, net or gross, per engine (lb)
V	T(4), S(4), VEL	- aircraft velocity (ft/sec)
V_x	S(10)	- horizontal component of V (ft/sec)
V_y	S(11)	- vertical component of V (ft/sec)
V_l	V1	- engine failure speed, EAS (knots)
V_R	VR	- rotation speed, EAS (knots)
W	W, WG	- aircraft weight (lb)
W_f	WF, WFUEL	- fuel flow (lb/hr)
α	ALPHA	- angle of attack (deg)
γ	S(5), GAMMA	- flight path angle (rad, deg)
δ_F	DELFD	- flap deflection (deg)
δ_s	DELSPL	- spoiler deflection (deg)

θ	THETAF	- pitch attitude fuselage angle (deg)
ν	ANGLE	- vectored thrust deflection angle (deg)
ρ	RHO	- air density (slugs/ft ³)
μ	MU	- rolling coefficient of friction
μ_{BRK}	XMUBRK	- braking coefficient of friction

SUBROUTINES

Subroutine TAKOFF

The subroutine TAKOFF simulates the takeoff maneuver of a given aircraft. The program is applicable to conventional, vectored lift and powered lift aircraft. The aircraft is treated as a point mass confined in motion to a vertical plane and the rotational dynamics are neglected. This simplification necessitates an estimation of all rotational rates involved. These rates are either input by the user or are approximated by a finite difference form.

The takeoff maneuver is divided into four basic segments: ground roll and rotation, liftoff and initial segment climb, acceleration to final climb speed at a constant rate of climb, and finally, the pullup maneuver to establish the final climb speed. Provisions in the program are made for gear retraction, flap retraction, changing of vectored thrust angle and changes in the power setting.

The ground roll is made at a specified power setting and flap deflection. When the rotation speed is reached, the aircraft is "rotated" by increasing the angle of attack linearly with time until liftoff occurs or the tail scrape angle is reached. If the latter occurs, the ground roll is continued with the fuselage angle equal to the tail scrape angle.

The flight path control is obtained by monitoring three dynamic variables — acceleration along flight path, load factor and fuselage angle (pitch attitude). The aircraft is not permitted to decelerate and the load factor and fuselage angle are restricted to values less than or equal to a specified value. If any of these conditions are violated, the angle of attack is reduced until all constraints are satisfied.

Once a specified altitude is attained, called the maneuvering altitude, the aircraft is pitched down by a reduction in angle of attack until a specified rate of climb is obtained. The aircraft then accelerates at this rate of climb until the desired final climb speed is reached.

When the final climb speed is attained, the pullup maneuver is executed in order to bring the aircraft to a zero rate of acceleration along the flight path. This maneuver is accomplished by increasing the angle of attack and pulling a load factor of 1.20, which will result in an increase in the rate of climb to a final value at the desired climb speed. It may be necessary to throttle the engines in order to maintain the desired constant climb speed subject to the fuselage angle restriction.

Program Inputs

The inputs to subroutine TAKOFF are through the argument list, input by NAMELIST and common blocks /UNIV/ and /AERO/.

The call to TAKOFF is as follows: CALL TAKOFF (INPC, IDCN, WGROSS, SWING, XENG, V1, VR, VEND) where

INPC	-	program control	=	1	-	input data loaded
			=	2	-	program executed
			=	3	-	data input and program executed
IDCN	-	print control	=	1	-	no print out
			=	9	-	print out
WGROSS	-	aircraft gross weight (lbs)				
SWING	-	reference wing area (sq ft)				

XENG	-	number of engines
V1	-	critical engine failure speed (knots)
VR	-	rotation speed (knots)
VEND	-	final climb speed (knots)

All speeds are indicated air speeds.

There are two namelist inputs to TAKOFF, /NAM1/ and /NAM2/.

The namelist /NAM1/ input variables are as follows:

CDGEAR	-	drag increment due to gear
DFLPDT	-	flap retraction rate (deg/sec)
DTABS	-	temperature increment above 59°F (°F)
DTGR	-	time required to retract gear (sec)
DTPDWN	-	throttling down rate (percent/sec)
DTPUP	-	throttling up rate (percent/sec)
DTVECT	-	vectored thrust angle reduction rate (deg/sec)
EYEWNG	-	wing incidence angle (deg)
HAPT	-	airport altitude (ft)
HGR	-	altitude at which gear retraction is started (ft)
HMAN	-	maneuvering altitude (ft)
HMAX	-	takeoff termination altitude (ft)
IOUT	-	for engine out takeoff, set IOUT = 1
UM	-	rolling coefficient of friction
NPAGE	-	no. of lines printed per page
PMARG	-	pullup speed margin
RTCL	-	rate of climb during accelerate segment (fpm)
THTFLY	-	maximum allowable fuselage angle while airborne (deg)
THTSCP	-	tail scrape angle (deg)

XLFXAX - maximum allowable load factor
DTFAIL - time required for one engine to fail (sec)

The user may input all, some, or none of the above input variables.
The default values of these input variables are listed below:

CDGEAR = 0.0, DFLPDT = 3.0 deg/sec, DTABS = 0.0°F,
DTGR = 5.0 sec, DTPDWN = 5.0 percent/sec,
DTPUP = 6.0 percent/sec, DTVECT = 10. deg/sec,
EYEWNG = 1.0 deg, HAPT = 0.0 ft, HGR = 25.0 ft,
HMAN = 1000. ft, IOUT = 0, UM = 0.02, PMARG = 0.04,
RTCL = 750. fpm, THTFLY = 15.0 deg,
THTSCP = 10. deg, XLFXAX = 1.15, DTFail = 3.0 sec

If the default value of CDGEAR is used, the program will calculate, based on an empirical formula, a value for the gear drag as a function of gross weight and wing area.

The second set of namelist variables, /NAM2/, constitute the flap, throttle and vectored thrust schedules. These are tables that manage the flap setting, power setting and vectored thrust angle as a function of the aircraft speed and altitude. These variables are arrays of dimension 5.

XDELFD(I) - flap deflection (deg)
XHFLAP(I) - flap retraction altitude (ft)
XVFLAP(I) - flap retraction speed (knots)
XPOWER(I) - power setting

XHPWR(I) - power setting change altitude (ft)
XVPWR(I) - power setting change speed (knots)
XNU(I) - vectored thrust angle (deg)
XHVECT(I)- vectored thrust angle change altitude (ft)
XVVECT(I)- vectored thrust angle change speed (knots)

All altitudes are absolute altitudes and all speeds are indicated air speeds.

These schedules are constructed as follows: If the speed or altitude of the aircraft is equal to, say, XVFLAP(I) or XHFLAP(I), respectively, then the flaps are retracted to the value XDEIFD(I). The power setting and vectored thrust angle management work in a similar manner. The power setting may either be increased or decreased. The flap setting and vectored thrust angle setting can only be reduced with speed and altitude. The values of XDEIFD(1), XNU(1) and XPOWER(1) are all for the ground run. The user is permitted four changes in flap, power, vectored thrust angle settings during the airborne portion of the takeoff.

The default values for /NAM2/ are as follows:

- 100. percent throttle throughout takeoff
- 0. degrees vectored thrust
- 15.0 degrees flaps during ground roll, retracted to 5.0 degrees at 250 ft altitude, retraction to 2.0 degrees at 200 knots, and finally, complete retraction at 210 knots

Again, the user may choose to use all, some, or none of the above schedule values. No changes to any of these settings are allowed during the pullup maneuver.

Program Output

The program output consists of a time history of several aircraft and flight path parameters. See sample listing presented in Appendix B. The variable DIST is the flight path track distance along the ground. The variable TAS is the true airspeed and EAS is the indicated airspeed. DALPH/DT and DTHTA/DT are the time rate of change of the angle of attack and fuselage angle respectively. In addition, the user may also obtain the following values through the common block /EXCHNG/:

SROLL	- distance to liftoff (ft)
S35	- track distance to 35 ft (ft)
V35	- speed (EAS) at 35 ft altitude (knots)
T5J	- ground distance covered by aircraft at time of engine failure

The variable T5J may be used in conjunction with the subroutine ROLL to calculate accelerate - stop distances.

The program will terminate normally when the end speed is reached (VEND) or when the maximum specified altitude (HMAX) is attained.

Abnormal termination will occur under several conditions:

- flight path constraints cannot be met by further reduction in angle of attack
- aircraft cannot accelerate at input rate of climb (RTCL)
- aircraft altitude goes negative

- ground track distance greater than 10. nautical miles
- ground run exceeds 90 seconds
- elapsed time greater than 300 seconds

For further definitions and explanations refer to the listing of TAKOFF and supporting subroutines contained in Appendix C, and the example case presented in Appendix B.

Subroutine LANDING

The subroutine LANDING simulates the landing maneuver of a given aircraft. As in the TAKOFF subroutine, the aircraft is treated as a point mass confined to motion in a vertical plane and the rotational dynamics are neglected. The landing is divided into three distinct phases: the approach, the flare to touchdown, and the rollout.

The landing approach is made at the thrust and angle of attack required for zero acceleration along and normal to the flight path. These values of thrust and angle of attack for the steady state approach may either be input by the user or calculated in subroutine ZERO.

The flare is executed by increasing the angle of attack at a specified rate (DADT). The program iterates on the flare initiation altitude until the rate of sink at touchdown equals a specified value (SINKTD).

Flight path control during the flare is obtained by monitoring the load factor, fuselage angle and pitch rate. These three variables are all restricted to values less than or equal to values specified by the user. If any of these conditions are violated, the angle of

attack is reduced until all constraints are satisfied. Provisions are made for spoiler retraction and increases in power setting during the flare if desired.

After the touchdown, the rollout is then executed, with provisions in the program for any pilot reaction or delay time, brake application, deployment of spoilers and thrust reversing. The landing run terminates when the aircraft comes to rest.

Program Inputs

The inputs to subroutine LANDNG are through the argument list, common blocks /UNIV/ and /AERO/ and namelist /NAM3/.

The call to LANDNG is as follows: CALL LANDNG (INPC, IWRITE, WGROSS, SWING, XENG, PWRSET, MODE, IZERO, IREV, NER) where

INPC	- program control	= 1 input data loaded
		= 2 program executed
		= 3 input data loaded and program executed
IWRITE	- print control	= 1 no print out
		= 2 print out
		= 3 iteration on HFLARE printed out
WGROSS	- aircraft gross weight (lbs)	
SWING	- reference wing area (sq ft)	
XENG	- number of engines	
PWRSET	- power setting	
MODE	- roll out option control (see below)	

IZERO - approach values of thrust and angle of
 attack = 0 calculated by program
 = 1 input by user

 IREV - reverse thrust control = 0 no reverse
 thrust
 = 1 reverse thrust
 used

 NER - error indicator = 1 successful case

The user has two options for the ground roll calculations. An average deceleration rate and delay time may be input and the ground roll distance determined by a single formula (MODE = 2). The second option is the time step integration (MODE = 1).

The namelist /NAM3/ input variables are as follows:

ABAR - average deceleration (g's)
 CDGEAR - drag increment due to gear
 DADT - time rate of change of angle of attack
 during flare (deg/sec)
 DTABS - temperature increment above 59°F (°F)
 DTDIMX - maximum allowable pitch rate during flare
 (deg/sec)
 DTPENG - throttling rate (percent/sec)
 FAAFTR - field length factor
 HAPP - approach screen height (ft)
 HAPT - altitude of airport (ft)
 HSPoil - minimum spoiler retraction altitude (ft)
 IPOWER - throttle modulation control
 ISPOIL - spoiler retraction control } see below
 PWRIDL - power setting at idle thrust
 PWRMAX - maximum power setting

PWRMRG	- power setting margin
SINKTD	- sink rate at touchdown (ft/sec)
TDELAY	- delay time after touchdown before any braking action taken (sec)
THEMAX	- maximum fuselage angle (deg)
TBRK	- time before brake application (sec)
TFLP	- time before flap retraction (sec)
TOFF	- time before engine shut down (sec)
TREV	- time before reverse thrust applied (sec)
TSPL	- time before spoilers deployed (sec)
XDIST	- desired landing distance (ft)
XMUBRK	- braking coefficient of friction
XLFMX	- maximum allowable load factor
QUESS	- see subroutine ZERO
HFLARE	- initial guess of flare altitude (ft)
STEP	- step size for iteration on HFLARE

in addition, the following are input through common block /LAND/

COMMON /LAND/ GAMAPP, VKAPP, ALPHMX

where

GAMAPP	- flight path angle, measured positive below horizon (deg)
VKAPP	- true airspeed at approach (knots)
ALPHMX	- maximum allowable angle of attack during flare, set equal to THEMAX in subroutine ZERO (deg)

The user may choose to input the approach speed (VKAPP) or input the desired landing distance (XDIST) and the program will calculate the required approach speed. This calculated approach speed is based on a constant load factor flare (XLFMAX) and the input values of ABAR, XLFMAX, GAMAPP, SINKTD and TDELAY. To use this option, the user should set VKAPP = 0. before the call to LANDNG.

The approach values of thrust per engine and angle of attack may be input (IZERO = 1) through common block /AERO/ or calculated by subroutine ZERO (IZERO = 0).

The guess for the flare initiation altitude can be input by the user or calculated by the program (use default value of HFLARE). The variable STEP controls the step size in the iteration to find the proper flare height. For powered - lift or any other aircraft that experience negative ground effects (suck-down), it is suggested that HFLARE and STEP be input as 40.0 ft and 0.9 respectively.

For ISPOIL = 0, the spoiler deflection angle (DELSPL) remains constant throughout the flare, and for IPOWER = 0, the throttle setting (PWRSET) is held fixed during the flare. For those aircraft experiencing negative ground effects, the spoilers may be retracted to obtain direct lift control (ISPOIL = 1) and the power setting advanced during the flare (IPOWER = 1). If the load factor during the flare should decrease, usually occurring when at or near maximum allowable angle of attack, the power setting will be advanced. Spoilers may be retracted when the aircraft is at an altitude of HSPoil or when $PWRMAX - PWRSET < PWRMRG$.

If the user chooses to use reverse thrust during the ground roll, he must supply a subroutine REVRSE, which returns the total force

coefficients along and normal to the ground roll velocity vector. It is envisioned that this subroutine would be similar in structure to subroutine ARODYN, using the same common blocks to transfer required variable values. When using reverse thrust, IREV = 1 must be input.

During the ground roll, the user may select to apply brakes, retract flaps, deploy spoilers, shut engines down or use reverse thrust, or any combination thereof. Following touchdown, there is a delay of TDELAY seconds during which time no braking action is taken. After this delay time interval has elapsed, the various braking techniques listed above may be employed, with additional time delays for each (TBRK, TFLP, TOFF, TREV, TSPL). Spoilers are extended at a rate of 90 degrees per second, 90 degrees being fully deployed, and flaps are retracted to zero degrees deflection at a rate of 10.0 degrees/sec. If no reverse thrust is used, the power setting is reduced to idle (PWRIDL) at the specified rate of DTPENG percent/sec. If reverse thrust is applied, the power setting is advanced to 100 percent at the specified rate of DTPENG percent/sec. If the user desires the flap setting, spoiler deflection or throttle setting to remain fixed at the value at touchdown, he should input a large value for the associated time delay interval (say, 100 seconds).

The user may input all, some, or none of the input variables discussed above. The default values of these variables are listed below.

ABAR = 0.35 g's, CDGEAR = 0.0, DADT = 5.0 deg/sec,
DTABS = 0.0 °F, DTDTMX = 7.0 deg/sec, DTPENG = 3.0
percent/sec, FAAFTR = 0.60, HAPP = 35.0 ft, HAPT
= 0.0 ft., THEMAY = 10.0 deg, TBRK = 0.0 sec,

TFLP = 0.0 sec, TOFF = 0.0 sec, TREV = 0.0 sec,
TSPL = 0.0 sec, XDIST = 5000 ft,
XMUBRK = 0.40, XLFMAX = 1.15, HFLARE = 0.0 ft,
STEP = 0.9

If the default value of CDGEAR is used, the program will calculate a value for the gear drag based on an empirical formula as a function of gross weight and wing area.

For further definitions and explanations refer to the listing of LANDNG and supporting subroutines contained in Appendix C, and the example case presented in Appendix B.

Subroutine ZERO

Given the aircraft configuration, its velocity and flight path angle, subroutine ZERO determines the required values of thrust per engine and angle of attack for zero acceleration along and normal to the flight path.

The mathematical problem entails driving two functions of two independent variables simultaneously to zero.

$$\text{Let } f(T, \alpha) = dV/dt$$

$$g(T, \alpha) = d\gamma/dt$$

where

T - engine thrust

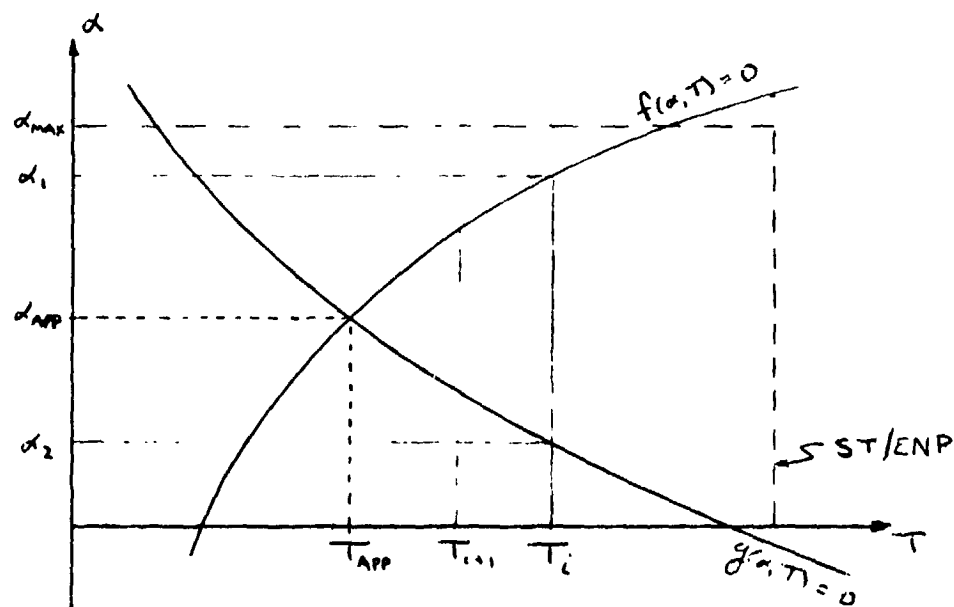
α - angle of attack

dV/dt - time rate of change of velocity along flight path

d γ /dt - time rate of change of flight path angle

Subroutine ZERO generates the locus of $f(T, \alpha) = 0$ and $g(T, \alpha) = 0$, and then searches for their intersection.

The values of thrust and angle of attack at this point are the required value for the steady state approach.



The above figure shows a typical plot of the f and g functions. The values α_{APP} and T_{APP} are the desired values of angle of attack and thrust. The upper bound on the thrust is the static sea level thrust. The search for α_1 and α_2 is made on the interval $-\alpha_{max} \leq \alpha_i \leq \alpha_{max}$, $i = 1, 2$. The error is then defined to be the difference between α_1 and α_2 . The subroutine varies the value of the thrust until the error is driven to zero, or $\alpha_1 = \alpha_2$. In varying the thrust, $T_{i+1} = T_i$ times STEP, where STEP is an input parameter, usually less than 1.0. The initial guess at the value of thrust is defined to be the sea level static thrust times the parameter QUESS:

$$T_1 = T_{SLS} * QUESS$$

It is suggested that the user make this initial guess of the thrust "high", so that the program does not search in areas where there is no solution of $f(\alpha, T) = 0$. Recommended values of QUESS are:

- 1) conventional aircraft — QUESS = 0.50
- 2) powered — lift — QUESS = 0.80

The default value for QUESS is 0.80. In the main calling program, the user must specify a value for the total sea level static thrust (ST) before the call to LANDNG is made.

Subroutine ZERO may also be used to determine the static performance of an aircraft, given its velocity and flight path angle. The flight path angle is measured positive below the horizon (i.e., if the aircraft is climbing at a flight path angle of 5.0 degrees, the call to ZERO would be made with GAMAPP = -5.0).

The call to ZERO would be as follows:

CALL ZERO (NER, EN, ALT, DTABS, KENG, PWRSET, QUESS)

where

NER	-	error indicator = 1 successful case
EN	-	aircraft Mach no.
ALT	-	aircraft altitude (ft)
DTABS	-	temperature increment above 59°F (°F)
KENG	=	1
PWRSET	-	power setting (returned)
QUESS	-	initial guess parameter

The following common blocks must also be used:

/UNIV/ - passes ENP, ST, W, etc.

/LAND/ - passes GAMAPP, ALPHMX

/AREO/ - passes QS, VEL, HABS

where

QS = product of dynamic pressure and wing area

VEL = aircraft speed (ft/sec)

HABS = absolute altitude of aircraft (ft)

Subroutines ENGINE and ARODYN are both called by ZERO. The call to ENGINE is made with KENG = 1 (see description of subroutine ENGINE). The user may choose to work either with gross thrust or net thrust, as long as he is consistent in the use of the variable "THRUST" in the definition of total force coefficients and power setting (PWRSET).

Subroutines ARODYN and ENGINE

The takeoff and landing subroutines described above require the user to provide two subroutines to compute total force coefficients and determine various required engine characteristics (e.g., thrust per engine and fuel flow). The format and structure of these subroutines is left to the discretion of the user.

I. Subroutine ARODYN

This subroutine computes the total force coefficients along the flight path and normal to the flight path as a function of angle of attack and thrust. A force coefficient in a particular direction is

defined to be the sum of all forces (excluding the weight component) in that particular direction divided by the dynamic pressure times the wing area.

$$C_x \equiv \frac{\vec{e}_x \cdot \Sigma \vec{F}}{qS}$$

The transfer of the various computer variables to and from subroutine ARODYN is through labeled common blocks /UNIV/ and /AERO/. Of primary concern is the common block /AERO/:

/AERO/ VEL, QS, HABS, THRUST, TVECT, ANGLE, DELFD, DELSPL,
ALPHA, CX, CY, CL, CD, RHO, GRCD, IFAST

The input variables from TAKOFF, LANDNG and ZERO are:

VEL	- aircraft velocity along flight path (ft/sec)
QS	- dynamic pressure time wing area (lbs)
HABS	- absolute altitude of aircraft (ft)
THRUST	- thrust (gross or net) per engine (lbs)
TVECT	- total vectored thrust (lbs)
ANGLE	- angle of vectored thrust relative to aircraft center line, positive down (deg)
DELF	- flap deflection (deg)
DELSPL	- spoiler deflection (deg)
ALPHA	- angle of attack (deg)
RHO	- air density (slugs/ft ³)
GRCD	- drag increment due to gear

The return from ARODYN should be:

CX - total force coefficient along flight path

CY - total force coefficient normal to flight path

The output variable CL and CD are provided to the user as a means to distinguish between pure aerodynamic coefficients and total force coefficients. The output variables CL and CD are printed out in the time histories, but are not used in the actual calculations. If desired, in subroutine ARODYN, CL and CD may be directly equated to CY and CX, respectively.

There is a certain amount of redundancy among some of the input variables. The user may utilize only those variables he desires and disregard the others. Due to the wide range of velocities encountered during the takeoff and landing maneuver, there will be a correspondingly large variation in the magnitude of the force coefficients which must be accommodated in subroutine ARODYN.

II. Subroutine ENGINE

This subroutine provides the various propulsion data to subroutines TAKOFF, ZERO and LANDNG.

The inputs to subroutine ENGINE are through the argument list and labeled common blocks /AERO/ and /UNIV/.

The call to ENGINE is as follows:

```
CALL ENGINE (ALT, DTABS, EN, PWRSET, WFUEL, KENG)
```

where

ALT - aircraft altitude

DTABS - temperature increment above 59°F (°F)

EN - aircraft Mach no.
PWRSET - power setting (see below)
WFUEL - fuel flow (lbs/hr)
KENG - engine control parameter (see below)

The variable PWRSET is defined to be:

$$PWRSET = \frac{\text{Net thrust}}{\text{Net thrust available}}$$

and is the parameter used in controlling the thrust level. It is used for power setting management during the takeoff (e.g. throttle cutback for noise abatement), thrust modulation during the landing flare, and is calculated for the steady state approach.

Used in conjunction with PWRSET is the variable KENG, the engine control parameter. For KENG = 0 or 2 (takeoff and landing respectively), the value of PWRSET is input and the thrust and fuel flow returned. In the static performance calculations of subroutine ZERO, the call to ENGINE is made with KENG = 1. Here, the thrust per engine is input and PWRSET and fuel flow are calculated.

The user may choose to work with either the gross thrust per engine or the net thrust per engine, provided he uses the variable THRUST properly in the calculation of the total force coefficients. For example, when using gross thrust per engine, the ram drag must be included in the total summation of forces. If the gross thrust vector and ram drag vector are collinear, the user may choose instead to work simply with the net thrust.

Refer to the example case presented for an illustration of subroutines ARODYN and ENGINE.

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1. Jim Webb, FLIGHT, The Iowa State University Press, Ames, 1971.
2. Susan E. Computer Programs for Estimation of STOL Takeoff, Landing, and Static Performance", NASA TM X-62,217, December 1972.

APPENDIX A

EQUATIONS

Equations used in TAKOFF and LANDNG

- 1) Equation of motion along flight path

$$dV/dt = (g/W)(-C_x qS - W \sin \gamma)$$

- 2) Equation of motion normal to flig. path

$$d\gamma/dt = (g/WV)(C_y qS - W \cos \gamma)$$

- 3) Equation of motion during ground roll

$$dV/dt = (g/W)[-W\mu + qS(C_{y\mu} - C_x)]$$

where

g = gravity constant

W = aircraft weight

q = dynamic pressure

S = wing area

γ = flight path angle

V = aircraft velocity

C_x = total force coefficient along flight path

C_y = total force coefficient normal to flight path

- 4) Load factor

$$XLF = \frac{qSC_y}{W \cos \gamma}$$

5) Constant rate of climb equation

$$\text{Rate of climb} \triangleq \text{ROC} = V \sin \gamma$$

For ROC to be constant with time,

$$\frac{d\text{ROC}}{dt} = 0$$

$$\therefore \frac{d\text{ROC}}{dt} = \frac{d}{dt} (V \sin \gamma)$$

$$= \frac{dV}{dt} \sin \gamma + V \cos \gamma \frac{d\gamma}{dt} = 0$$

Substitute for terms dV/dt and $d\gamma/dt$ from equations 1) and 2)

$$\begin{aligned} (g/W)(-C_x qS - W \sin \gamma) \sin \gamma \\ + V \cos \gamma (g/WV)(C_y qS - W \cos \gamma) \cos \gamma = 0 \end{aligned}$$

$$-C_x qS \sin \gamma - W \sin^2 \gamma + C_y qS \cos \gamma - W \cos^2 \gamma = 0$$

or

$$qS (C_y \cos \gamma - C_x \sin \gamma) - W = 0$$

6) Rotational rate approximations by finite difference

$$\theta = \gamma + \alpha - i_w$$

where

θ - pitch attitude (fuselage angle)

γ - flight path angle

α - angle of attack

i_w - incidence of wing

Differentiating with respect to time we obtain:

$$\frac{d\theta}{dt} = \frac{d\alpha}{dt} + \frac{dy}{dt}$$

where $\frac{dy}{dt}$ is given by equation 2).

$\frac{d\alpha}{dt}$ is approximated by the finite difference form:

$$\frac{d\alpha}{dt} = (\alpha_{\text{now}} - \alpha_{\text{past}}) / \Delta t$$

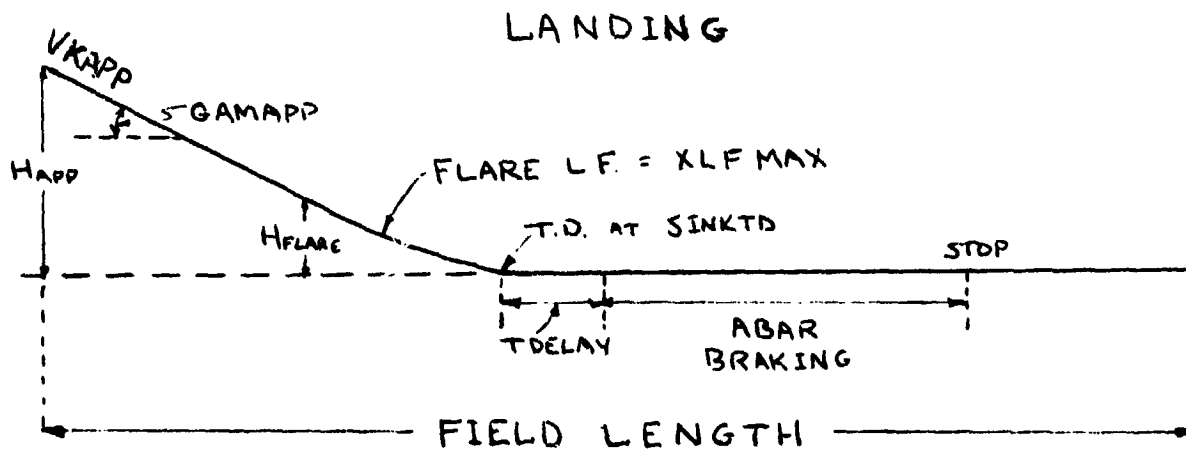
where

α_{now} = current value of angle of attack

α_{past} = previous value of angle of attack

Δt = integration time interval

- 7) Simplified landing equations - for constant load factor (XLF_{max}),
constant speed (V_{App}) flare



where: $R = \frac{V_{APP}^2}{g(XLF_{max} - 1.0)}$

$$h_{flare} = \frac{V_{APP}^2 (\gamma_{APP}^2 - \gamma_{TD}^2)}{2g (XLF_{max} - 1.0)}$$

and

$$XDIST = \frac{35.0}{\tan \gamma_{APP}} + \frac{R \gamma_{APP}}{2} \left(1.0 - \frac{\gamma_{TD}}{\gamma_{APP}} \right)^2$$

$$+ V_{APP} t_{DELAY} + \frac{V_{APP}^2}{2g \cdot \bar{a}}$$

where

t_{DELAY} - delay time before braking

\bar{a} - average deceleration (g's)

APPENDIX B

SAMPLE CASE

Shown below is an example of the input, calling format, sub-routines ARODYN and ENGINE, and the print out obtained for the takeoff and landing programs.

The main calling program TEST1 is set up to do the takeoff and landing of a Boeing 727-200. The required common blocks are shown, but others may be added if required. Note that the spoiler deflection angle DELSPL has been set equal to zero before the call to TAKOFF. Also note that before calling the landing program, the flap deflection DELFD, the spoiler deflection DELSPL and the total static sea level thrust ST must be given values externally to LANDNG.

The namelist input was as follows:

```
$NAM1 NPAGE = 48, RTCL = 530., THTFLY = 20., HMAN = 2000. $END
```

```
$NAM2 XPOWER(2) = 0.75, XHPWR(2) = 750., XPOWER(3) = 0.95
```

```
XHPWR(3) = 1750. $END
```

```
$NAM3 DADT = 1.0, IPOWER = 0, TFLP = 99., PWRIDL = 0.10,
```

```
SINKTD = 3.0, TOFF = 3.0, TSPL = 2.00, XMUBRK = 0.45 $END
```

Subroutine ARODYN calculates the lift and drag coefficients of the 727-200 as a function of angle of attack, flap and spoiler deflection. The increments of lift and drag due to flaps is determined in a table look-up format. The increase in drag and loss in lift increment due to

spoilers is assumed to vary linearly with spoiler deflection. Once the lift and drag coefficients are computed, the thrust components, normalized with respect to dynamic pressure times wing area ($Q S$), are added in to determine the total force coefficients C_X and C_Y .

Subroutine ENGINE computes the thrust and fuel flow of the JT8D engine, based on a simplified model. The thrust lapse is assumed to be linear with Mach number, and the fuel flow assumed linear with power setting. Note the use of the parameter PWRSET. The subroutine consists basically of two sections. For KENG = 0 or 2, the power setting PWRSET is input and the thrust and fuel flow returned. For KENG = 1, the thrust is input and PWRSET and fuel flow returned. No reverse thrust was used during the landing ground roll and subroutine REVRSE is simply a dummy subroutine.

This particular run was made on the Lawrence Berkeley Laboratory CDC 7600 and required a CPU time of 2.38 seconds.

TEST1

```

PROGRAM TEST1(INPUT,OUTPUT,TAPES=INPUT,TAPE6=OUTPUT)
COMMON /UNIV/ NPC ,NSC ,IDC ,H ,ST ,R ,W ,
1WF ,EM ,VMO ,EMH0 ,ALPHLO,CLALPH,SW ,AR ,B ,
2EYEW ,ENP ,TA ,WG ,WGS ,KWRITE,OLMC4
3*KSIZ
COMMON /AERO/ VEL,GS,HABS,THRUST,TVECT, ANGLE,DELFD,DELSPL,A1 PHA,
9CX,CY,CL,CD,RHO,GRCD,IFAST
COMMON/LAND/ GAMAPP,VKAPP,ALPHMX
COMMON /EXCHNG/ SROLL,SJS,Y35,T5J
WRITE(6,100)
100 FORMAT(1H1,///)
6 WG = 17200.
7 SWING = 1720.
11 ENP = 3.0
12 V1 = 125.
14 VR = 135.
15 VEND = 250.
17 DELSPL = 0.0
20 CALL TAKOFF(3,9,WG,SWING,ENP,V1,VR,VEND)
27 DELSPL = 0.0
30 DELFD = 40.
31 WG = 15000.
33 CT = 42000.
34 VKAPP = 130.
36 GAMAPP = 3.0
40 CALL LANDING(3,2,WG,SWING,ENP,PWRSET,i,i,0,NER)
51 END

```

PROGRAM LENGTH INCLUDING I/O BUFFERS

01165

FUNCTION ASSIGNMENTS

STATEMENT ASSIGNMENTS

100 - 000065

BLOCK NAMES AND LENGTHS

UNIV - 000030/01 AERO - 000020/02 LAND - 000003/03 EXCHNG - 000004/04

VARIABLE ASSIGNMENTS

DELFD - 000006/02 DELSPL - 000007/02 ENP - 000021/01 GAMAPP - 000000/03 NER - 000116 PWRSET - 000115
ST - 000004/01 SWING - 000111 VEND - 000114 VKAPP - 000001/03 VR - 000112
WG - 000023/01

START OF CONSTANTS-000054 TEMPS--000107 INDIRECTS-000111

7600 COMPILATION -- RUN76 LEVEL 5C 73/07/04.

ROUTINE COMPILES IN 044000

ARODYN

```

SUBROUTINE ARODYN
  REAL NU
  COMMON /UNIV/ NPC ,NSC ,IDC ,H ,ST ,R ,W ,
  IMF ,EM ,VMO ,ALPHLO,CLALPH,SM ,AR ,B ,
  ZEYEW ,ENP ,TA ,WG ,WRITE,OLMC,
  3,KSIZE
  COMMON /AERO/ VEL,QS,HABS,THRUST,IVECT, ANGLE,DELFD,DELSPL,ALPHA,
  9,CX,CY,CL,CD,RHO,GRC,IFAST
  DIMENSION XDELFD(6),XDELCL(6),XDELCD(6),XVDEL6(6)
  DATA XDELFD/0.0,0.5,0.10,0.15,0.20,0.25,/
  DATA XDELCL/0.0,0.186,0.347,0.482,0.60,0.702/
  DATA XDELCD/0.0,0.0148,0.0295,0.0451,0.0607,0.0837/
  DATA XVDEL6/1.0,0.995,0.990,0.980,0.970,0.955/
  IF(IFAST .EQ. 1) GO TO 1
  CALL ITRLN(XDELFD,XDELCD,XDELCL,DELFD,DELCDF,6)
  CALL ITRLN(XDELFD,XDELCL,XDELCD,DELFD,DELCDF,6)
  CALL ITRLN(XDELFD,XVDEL6,DELFD,VDEL6,6)
  SAS = 0.016
  CLALPH = 4.5
  ALPHLO = -1.5
  SAT = 0.0546
  SIGMA = 0.6
  DCLSP = 0.31*(DELSPL/90.)
  DCDSPL = 0.12*(DELSPL/90.)
  CL = CLALPH*(ALPHA - ALPHLO)*0.017453 + DELCLF
  CL = CL - DCLSP
  CD = SAS + DELCDF *(SAT/VDEL6)*(CL - SIGMA*DELCLF)**2 + GRCD
  CD = CD + DCDSPL
  1 ALPHA = ALPHA + .0174533
  IF(QS .EQ. 0.0)QS = 0.1
  CX = CD - THRUST*ENP*COS(ALPHX)/QS
  CY = CL + THRUST*ENP*SIN(ALPHX)/QS
  RETURN
END

```

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SUBPROGRAM LENGTH

00171

FUNCTION ASSIGNMENTS

STATEMENT ASSIGNMENTS

1 - 000054

BLOCK NAMES AND LENGTHS

UNIV - 000030/01 AERO - 000020/02

VARIABLE ASSIGNMENTS

ALPHA - 000010/02	ALPHLO - 000013/01	ALPHX - 000170	CD - 000014/02	CL - 000013/02	CLALPH - 000014/01
CX - 000011/02	CY - 000012/02	DCDSPL - 000167	DCLSPL - 000166	DELCDF - 000160	DELCLF - 000161
DELFD - 000006/02	DELSPL - 000007/02	ENP - 000021/01	GRCD - 000016/02	IFAST - 000017/02	NU - 000127
QS - 000001/02	SAS - 000163	SAT - 000164	SIGMA - 000165	THRUST - 000003/02	VDEL6 - 000162
XDELCD - 000144	XDELCL - 000136	XDELFD - 000130	XVDEL6 - 000152		

```

ENGINE
      SUBROUTINE ENGINE(ALT,DTABS,EN,PWRSET,WFUEL,KENG)
      CCAMON /AERO/ VEL(QS,HABS,THRUST,TVECT, ANGLE,DELF0,DELSPL,ALPHA,
      9CX,CY,CL,CD,RHO,GRCD,IFAST
      IF(KENG.EQ. 1)GO TO 10
      TD = 14000.
      THRUST = (TO - 6.0*EN*1100.)*PWRSET
      11 WFUEL = THRUST*0.63*PWRSET
      16 RETURN
      20 PWRSET = THRUST/(TC - 6.0*EN*1100.)
      21 GO TO 11
      25 END
      26

```

SUBPROGRAM LENGTH

00043

FUNCTION ASSIGNMENTS

STATEMENT ASSIGNMENTS
10 - 000022 11 - 000017

BLOCK NAMES AND LENGTHS
AERO - 000020/01

VARIABLE ASSIGNMENTS
THRUST - 000003/01 TO - 000042

START OF CONSTANTS-000031 TEMPS--000036 INDIRECTS-000042

7600 COMPILATION -- RUN76 LEVEL 5C 73/07/04.

ROUTINE COMPILES IN 044000

REVRSE		SUBROUTINE REVRSE	
		RETURN	
	2	END	
SUBPROGRAM LENGTH			
00010			
FUNCTION ASSIGNMENTS			
STATEMENT ASSIGNMENTS			
BLOCK NAMES AND LENGTHS			
VARIABLE ASSIGNMENTS			
START OF CONSTANTS-000005	TEMPS--000006	INDIRECTS-000010	
7600 COMPILATION -- RUN76 LEVEL 5C	73/07/04.		
ROUTINE COMPILES IN 044000			

** INPUTS TO TAKE OFF - ALTITUDE = 0.0 TEMPERATURE = 59.0 DEG. F
 A/C CHARACTERISTICS
 GROSS RAMP WT. = 172000 WING AREA = 1720 STATIC SEA LEVEL THRUST = 14000
 WING LOADING = 100.0 THRUST/WEIGHT = .244
 A/C PARAMETERS,
 NO. ENGINES = 3.0 CDGEAR = .0287 EYEWNG = 1.0 TAIL SCRAPE ANGLE = 10.0
 FLIGHT PATH CONTROL PARAMETERS
 MAX LOAD FACTOR = 1.10 GEAR RETRACTION ALT. = 25.0 MAX FLOOR ANGLE = 20.0
 MANEUVER ALT. = 2000 ACCELERATE RATE OF CLIMB = 530
 PARAMETER VARIATION RATES
 OADT = 1.0 DFLPDT = 3.0 DTGR = 5.0 DTPDWN = 5.0
 DTDUP = 6.0 DTVECT = 10.0 DTFAIL = 3.0

POWER, VECTORED THRUST, AND FLAP SCHEDULES

THROTTLE/POWER SETTING			
PWRSET	1.00	.75	.95
SPEED	0.0	0.0	0.0
ALTITUDE	0	750	1750
			0

VECTORED THRUST ANGLE			
ANGLE	0.0	0.0	0.0
SPEED	0.0	999.0	999.0
ALTITUDE	0	0	0
			0

FLAP DEFLECTION ANGLE			
DELFO	15.0	5.0	2.0
SPEED	0.0	0.0	200.0
ALTITUDE	0	250	0
			0

ALL SPEEDS ARE INDICATED AIR SPEEDS AND ALL ALTITUDES ARE ABSOLUTE ALTITUDES

TAKEOFF (ELEVATION = 0 FT)

TIME (SEC)	DIST. (FEET)	WEIGHT (LBS)	ALT. (FEET)	TAS (KTS)	EAS (KTS)	MACH NO.	ACCEL (FPS ²)	CL	CD	ALPHA (DEG)	GAMMA (DEG)	R/C (FPM)	LOAD FACT	THRUST (LBS)	FUS. ANG.	DALPH /DT	DTHTA /DT
0.0	0.0	172000	0.0	0.0	0.0	0.000	7.22	.678	.0982	1.00	0.00	0.0	0.00	42000	0.0	0.00	0.00
1.0	3.6	171993	0.0	4.3	4.3	.006	7.20	.678	.0982	1.00	0.00	0.0	0.00	41885	0.0	0.00	0.00
2.0	14.4	171985	0.0	8.5	8.5	.019	7.17	.678	.0982	1.00	0.00	0.0	0.00	41757	0.0	0.00	0.00
3.0	32.4	171978	0.0	12.8	12.8	.038	7.14	.678	.0982	1.00	0.00	0.0	0.00	41630	0.0	0.00	0.00
4.0	57.5	171971	0.0	17.0	17.0	.055	7.10	.678	.0982	1.00	0.00	0.0	0.00	41504	0.0	0.00	0.00
5.0	89.7	171964	0.0	21.2	21.2	.071	7.06	.678	.0982	1.00	0.00	0.0	0.00	41378	0.0	0.00	0.00
6.0	129.0	171956	0.0	25.3	25.3	.088	7.02	.678	.0982	1.00	0.00	0.0	0.00	41253	0.0	0.00	0.00
7.0	175.3	171949	0.0	29.5	29.5	.104	6.98	.678	.0982	1.00	0.00	0.0	0.00	41129	0.0	0.00	0.00
8.0	228.6	171942	0.0	33.6	33.6	.120	6.93	.678	.0982	1.00	0.00	0.0	0.00	41005	0.0	0.00	0.00
9.0	288.8	171935	0.0	37.7	37.7	.136	6.88	.678	.0982	1.00	0.00	0.0	0.00	40882	0.0	0.00	0.00
10.0	355.9	171928	0.0	41.8	41.8	.153	6.83	.678	.0982	1.00	0.00	0.0	0.00	40761	0.0	0.00	0.00
11.0	429.8	171920	0.0	45.8	45.8	.169	6.78	.678	.0982	1.00	0.00	0.0	0.00	40640	0.0	0.00	0.00
12.0	510.5	171913	0.0	49.8	49.8	.185	6.72	.678	.0982	1.00	0.00	0.0	0.00	40520	0.0	0.00	0.00
13.0	597.9	171906	0.0	53.7	53.7	.201	6.66	.678	.0982	1.00	0.00	0.0	0.00	40401	0.0	0.00	0.00
14.0	692.0	171899	0.0	57.7	57.7	.217	6.60	.678	.0982	1.00	0.00	0.0	0.00	40283	0.0	0.00	0.00
15.0	792.6	171892	0.0	61.5	61.5	.233	6.53	.678	.0982	1.00	0.00	0.0	0.00	40167	0.0	0.00	0.00
16.0	898.8	171885	0.0	65.4	65.4	.249	6.46	.678	.0982	1.00	0.00	0.0	0.00	40051	0.0	0.00	0.00
17.0	1013.5	171878	0.0	69.2	69.2	.264	6.40	.678	.0982	1.00	0.00	0.0	0.00	39937	0.0	0.00	0.00
18.0	1131.5	171871	0.0	73.0	73.0	.280	6.33	.678	.0982	1.00	0.00	0.0	0.00	39824	0.0	0.00	0.00
19.0	1259.9	171864	0.0	76.7	76.7	.295	6.25	.678	.0982	1.00	0.00	0.0	0.00	39712	0.0	0.00	0.00
20.0	1392.6	171857	0.0	80.4	80.4	.311	6.18	.678	.0982	1.00	0.00	0.0	0.00	39602	0.0	0.00	0.00
21.0	1531.4	171850	0.0	84.0	84.0	.326	6.10	.678	.0982	1.00	0.00	0.0	0.00	39493	0.0	0.00	0.00
22.0	1676.3	171843	0.0	87.6	87.6	.342	6.03	.678	.0982	1.00	0.00	0.0	0.00	39385	0.0	0.00	0.00
23.0	1827.3	171837	0.0	91.1	91.1	.357	5.95	.678	.0982	1.00	0.00	0.0	0.00	39278	0.0	0.00	0.00
24.0	1984.2	171830	0.0	94.6	94.6	.373	5.87	.678	.0982	1.00	0.00	0.0	0.00	39173	0.0	0.00	0.00
25.0	2146.9	171823	0.0	98.1	98.1	.388	5.79	.678	.0982	1.00	0.00	0.0	0.00	39070	0.0	0.00	0.00
26.0	2315.5	171816	0.0	101.5	101.5	.404	5.71	.678	.0982	1.00	0.00	0.0	0.00	38968	0.0	0.00	0.00
27.0	2489.8	171809	0.0	104.9	104.9	.419	5.62	.678	.0982	1.00	0.00	0.0	0.00	38867	0.0	0.00	0.00
28.0	2669.6	171802	0.0	108.2	108.2	.435	5.54	.678	.0982	1.00	0.00	0.0	0.00	38768	0.0	0.00	0.00
29.0	2855.1	171796	0.0	111.4	111.4	.450	5.46	.678	.0982	1.00	0.00	0.0	0.00	38670	0.0	0.00	0.00
30.0	3046.0	171789	0.0	114.6	114.6	.466	5.37	.678	.0982	1.00	0.00	0.0	0.00	38574	0.0	0.00	0.00
31.0	3242.2	171782	0.0	117.8	117.8	.481	5.29	.678	.0982	1.00	0.00	0.0	0.00	38479	0.0	0.00	0.00
32.0	3443.8	171775	0.0	120.9	120.9	.497	5.20	.678	.0982	1.00	0.00	0.0	0.00	38386	0.0	0.00	0.00
33.0	3650.5	171769	0.0	123.9	123.9	.512	5.11	.678	.0982	1.00	0.00	0.0	0.00	38294	0.0	0.00	0.00
34.0	3862.4	171762	0.0	126.9	126.9	.528	5.03	.678	.0982	1.00	0.00	0.0	0.00	38204	0.0	0.00	0.00
35.0	4079.3	171755	0.0	129.9	129.9	.543	4.94	.678	.0982	1.00	0.00	0.0	0.00	38115	0.0	0.00	0.00
36.0	4301.1	171749	0.0	132.8	132.8	.559	4.85	.678	.0982	1.00	0.00	0.0	0.00	38028	0.0	0.00	0.00
AND TAS = 135.1 EAS = 135.11																	
37.0	4527.8	171742	0.0	135.6	135.6	.575	4.76	.694	.0989	1.20	0.00	0.0	0.00	37943	.2	1.00	1.00
38.0	4759.2	171735	0.0	138.4	138.4	.591	4.62	.773	.1028	2.20	0.00	0.0	0.00	37859	1.2	1.00	1.00
39.0	4995.3	171729	0.0	141.1	141.1	.607	4.47	.851	.1074	3.20	0.00	0.0	0.00	37778	2.2	1.00	1.00
40.0	5235.8	171722	0.0	143.7	143.7	.623	4.29	.930	.1127	4.20	0.00	0.0	0.00	37700	3.2	1.00	1.00
41.0	5480.6	171716	0.0	146.2	146.2	.639	4.09	1.008	.1186	5.20	0.00	0.0	0.00	37625	4.2	1.00	1.00
42.0	5729.5	171709	0.0	148.5	148.5	.655	3.87	1.087	.1252	6.20	0.00	0.0	0.00	37554	5.2	1.00	1.00
43.0	5982.3	171702	0.0	150.8	150.8	.671	3.63	1.165	.1326	7.20	0.00	0.0	0.00	37487	6.2	1.00	1.00
DIST = 6212.9 TAS = 152.6 EAS = 152.61																	
44.0	6238.8	171696	0.0	152.8	152.8	.687	3.35	1.244	.1406	8.20	.01	3.0	1.02	37424	7.2	1.00	1.11
45.0	6498.6	171689	.8	154.7	154.7	.703	2.79	1.311	.1479	9.05	.46	125.9	1.10	37369	8.5	-0.00	.69
46.0	6761.3	171683	4.5	156.2	156.2	.719	2.40	1.287	.1553	8.75	1.15	317.9	1.10	37322	8.9	-0.00	.69
47.0	7026.3	171676	11.4	157.5	157.5	.735	2.02	1.263	.1627	8.45	1.83	510.4	1.10	37282	9.3	-5.00	.18
48.0	7293.1	171670	21.6	158.6	158.6	.751	1.63	1.248	.1700	8.25	2.51	703.9	1.10	37249	9.8	-5.00	.15

TAKEOFF CONTINUED

TIME (SEC)	DIST. (FEET)	WEIGHT (LBS)	ALT. (FEET)	IAS (KTS)	EAS (KTS)	MACH NO.	ACCEL (FPS ²)	CL	CD	ALPHA (DEG)	GAMMA (DEG)	R/C (FPM)	LOAD FACT	THRUST (LBS)	FUS. ANG.	DALPH /DT	OTHTA /DT
GEAR RETRACTION STARTED AT 48.3 SEC. COMPLETE AT 53.3 SEC																	
49.0	7561.5	171663	34.9	159.5	159.4	.241	1.34	1.236	.1363	8.10	3.18	896.5	1.10	37222	10.3	-0.0	.67
DISTANCE TO 35 FT. = 7563.3 SCREEN SPEED (EAS) = 159.4 KNOTS																	
50.0	7931.0	171657	51.5	160.2	160.1	.242	1.12	1.224	.1293	7.95	3.65	1090.1	1.10	37200	10.8	-0.0	.66
51.0	8101.3	171650	71.2	160.8	160.6	.243	.91	1.216	.1228	7.85	4.52	1293.4	1.10	37181	11.4	-0.0	.67
52.0	8372.4	171644	94.2	161.3	161.0	.244	.70	1.208	.1162	7.75	5.18	1475.8	1.10	37166	11.9	-0.0	.66
53.0	8643.8	171637	120.4	161.6	161.3	.245	.49	1.205	.1101	7.70	5.84	1667.7	1.10	37154	12.5	-0.0	.67
54.0	8915.4	171631	149.4	161.8	161.5	.245	.20	1.201	.1074	7.65	6.50	1857.9	1.10	37147	13.2	-0.0	.67
55.0	9186.8	171624	182.3	161.9	161.5	.245	.01	1.154	.1027	7.05	7.09	2025.8	1.06	37145	13.1	-1.00	-.59
56.0	9458.1	171618	216.7	161.9	161.4	.245	.00	1.114	.0990	6.55	7.32	2089.8	1.02	37144	12.9	-0.0	.12
FLAPS RETRACTED TO 5.0 DEG. IN 3.3 SEC.																	
57.0	9729.2	171611	251.7	161.1	161.3	.245	.01	1.099	.0976	6.35	7.39	2108.9	1.00	37143	12.7	-0.50	-.46
58.0	10000.4	171605	286.9	161.9	161.3	.245	.13	1.096	.0923	7.35	7.41	2116.7	1.00	37142	13.8	1.00	1.03
59.0	10271.7	171598	322.3	162.0	161.3	.246	.24	1.088	.0871	8.35	7.44	2127.0	1.00	37138	14.8	1.00	1.02
60.0	10543.2	171592	357.7	162.2	161.4	.246	.38	1.070	.0822	9.35	7.42	2122.2	.99	37132	15.8	1.00	.94
61.0	10815.1	171585	393.0	162.4	161.5	.246	.22	1.117	.0862	10.35	7.45	2133.6	1.04	37125	16.8	1.00	1.22
62.0	11087.0	171579	429.5	162.5	161.5	.246	.00	1.121	.0867	10.40	7.81	2237.0	1.04	37123	17.2	-0.50	-.21
63.0	11358.8	171572	467.2	162.5	161.4	.246	.01	1.093	.0837	10.05	7.98	2285.5	1.01	37122	17.0	-0.0	.10
64.0	11630.5	171566	505.5	162.5	161.3	.246	.00	1.085	.0828	9.95	8.04	2302.6	1.01	37121	17.0	-0.0	.04
65.0	11902.2	171559	543.9	162.5	161.2	.246	.01	1.081	.0824	9.90	8.06	2308.1	1.00	37121	17.0	-0.0	.01
66.0	12173.9	171553	582.4	162.5	161.1	.246	.00	1.081	.0824	9.90	8.07	2311.1	1.00	37120	17.0	-0.0	.01
67.0	12445.6	171546	620.9	162.5	161.0	.247	.00	1.081	.0824	9.90	8.07	2312.2	1.00	37119	17.0	-0.0	.00
68.0	12717.3	171540	659.5	162.5	160.9	.247	.01	1.081	.0824	9.90	8.07	2311.3	1.00	37118	17.0	-0.0	-.01
69.0	12989.0	171533	698.0	162.5	160.8	.247	.00	1.085	.0828	9.95	8.06	2309.8	1.00	37118	17.0	-0.50	.49
70.0	13260.8	171527	736.5	162.5	160.8	.247	.00	1.085	.0828	9.95	8.06	2309.5	1.00	37117	17.0	-0.0	.00
RETARD THROTTLE SETTING TO 75.0 PERCENT IN 5.0 SEC.																	
71.0	13532.5	171520	774.9	162.5	160.7	.247	.01	1.038	.0779	9.35	7.96	2281.5	.95	36003	16.3	-1.00	-1.27
72.0	13804.5	171515	811.9	162.5	160.6	.247	.00	1.007	.0748	8.95	7.53	2157.0	.92	34146	15.5	-0.0	-.53
73.0	14076.7	171509	846.6	162.5	160.5	.247	.00	.999	.0740	8.85	6.95	1993.9	.91	32290	14.8	-0.0	-.60
74.0	14349.4	171505	878.3	162.5	160.4	.247	.00	.999	.0740	8.85	6.34	1820.0	.91	30434	14.2	-0.0	-.62
75.0	14622.3	171501	907.2	162.5	160.4	.247	.00	1.003	.0744	8.90	5.71	1639.4	.91	28577	13.6	-0.0	-.14
76.0	14895.1	171497	933.1	162.5	160.3	.247	.03	1.050	.0701	9.50	5.17	1483.2	.95	27835	13.7	1.00	.63
77.0	15169.0	171493	957.3	162.5	160.3	.247	.01	1.089	.0832	10.00	4.98	1428.6	.98	27834	14.0	-0.0	-.11
78.0	15442.5	171490	980.9	162.5	160.2	.247	.01	1.101	.0845	10.15	4.91	1410.3	.99	27834	14.1	-0.0	-.05
79.0	15716.1	171486	1004.3	162.5	160.2	.247	.01	1.105	.0849	10.20	4.89	1403.9	1.00	27833	14.1	-0.50	-.51
80.0	15989.5	171483	1027.7	162.5	160.1	.247	.01	1.109	.0854	10.25	4.88	1401.5	1.00	27833	14.1	-0.0	-.01
81.0	16263.1	171479	1051.0	162.5	160.1	.247	.01	1.109	.0854	10.25	4.87	1399.4	1.00	27833	14.1	-0.0	-.00
82.0	16536.6	171475	1074.4	162.5	160.0	.247	.00	1.113	.0858	10.30	4.87	1399.1	1.00	27832	14.2	-0.50	.49
83.0	16810.2	171472	1097.7	162.6	160.0	.247	.00	1.113	.0858	10.30	4.87	1398.7	1.00	27832	14.2	-0.0	.00
84.0	17083.7	171468	1121.0	162.6	159.9	.247	.00	1.113	.0858	10.30	4.87	1399.7	1.00	27831	14.2	-0.0	.00
85.0	17357.3	171464	1144.3	162.6	159.9	.247	.01	1.113	.0858	10.30	4.87	1398.6	1.00	27831	14.2	-0.0	-.00
86.0	17630.8	171461	1167.6	162.6	159.8	.247	.01	1.113	.0858	10.30	4.87	1398.2	1.00	27831	14.2	-0.0	-.01
87.0	17904.4	171457	1190.9	162.6	159.8	.247	.01	1.113	.0858	10.30	4.87	1397.6	1.00	27830	14.2	-0.50	-.49
88.0	18178.0	171453	1214.2	162.6	159.7	.247	.01	1.113	.0858	10.30	4.87	1397.4	1.00	27829	14.2	-0.0	-.01
89.0	18451.6	171450	1237.5	162.6	159.7	.247	.00	1.117	.0862	10.35	4.87	1397.7	1.00	27829	14.2	-0.0	.00
90.0	18725.2	171446	1260.8	162.6	159.6	.247	.00	1.117	.0862	10.35	4.87	1398.6	1.00	27829	14.2	-0.0	.00
91.0	18998.8	171442	1284.1	162.6	159.5	.247	.00	1.117	.0862	10.35	4.87	1398.3	1.00	27829	14.2	-0.0	-.00
92.0	19272.4	171439	1307.4	162.6	159.5	.247	.01	1.117	.0862	10.35	4.86	1396.9	1.00	27828	14.2	-0.0	-.01
93.0	19546.0	171435	1330.7	162.6	159.4	.247	.01	1.117	.0862	10.35	4.86	1395.9	1.00	27828	14.2	-0.50	-.49
94.0	19819.6	171431	1354.0	162.6	159.4	.247	.01	1.117	.0862	10.35	4.86	1395.5	1.00	27828	14.2	-0.50	-.50
95.0	20093.2	171428	1377.2	162.6	159.3	.247	.00	1.121	.0867	10.40	4.86	1395.7	1.00	27827	14.3	-0.0	.00
96.0	20366.8	171424	1400.5	162.6	159.3	.247	.00	1.121	.0867	10.40	4.86	1396.4	1.00	27827	14.3	-0.0	.00

TAKEOFF CONTINUED

TIME (SEC)	DIST. (FEET)	WEIGHT (LBS)	ALT. (FEET)	TAS (KTS)	EAS (KTS)	MACH NO.	ACCEL (FPS ²)	CL	CO	ALPHA (DEG)	GAMMA (DEG)	R/C (FPM)	LOAD FACT	THRUST (LBS)	FUS. ANG.	DALPH /DT	DTHTA /DT
97.0	20360.5	171420	1423.7	162.6	159.2	.247	.01	1.121	.0867	10.40	4.86	1396.0	1.00	27826	14.3	-0.00	-0.00
98.0	20914.1	171417	1470.2	162.6	159.2	.247	.00	1.121	.0867	10.40	4.85	1394.4	1.00	27826	14.3	-0.00	-0.01
99.0	21187.8	171413	1470.2	162.6	159.1	.247	.00	1.125	.0871	10.45	4.85	1393.8	1.00	27826	14.3	.50	.49
100.0	21461.4	171409	1493.5	162.6	159.1	.247	.00	1.125	.0871	10.45	4.85	1393.4	1.00	27825	14.3	.50	.49
101.0	21735.1	171406	1516.7	162.6	159.0	.247	.00	1.125	.0871	10.45	4.85	1393.9	1.00	27825	14.3	-0.00	.00
102.0	22008.8	171402	1539.9	162.6	159.0	.248	.00	1.125	.0871	10.45	4.85	1394.5	1.00	27825	14.3	-0.00	.00
103.0	22282.5	171399	1563.2	162.6	158.9	.248	.01	1.125	.0871	10.45	4.85	1393.9	1.00	27824	14.3	-0.00	.00
104.0	22556.1	171395	1586.4	162.6	158.8	.248	.01	1.125	.0871	10.45	4.85	1392.2	1.00	27824	14.3	-0.00	.01
105.0	22829.8	171391	1609.6	162.6	158.8	.248	.01	1.125	.0871	10.45	4.85	1392.2	1.00	27823	14.3	-0.00	.01
106.0	23103.5	171388	1632.8	162.6	158.8	.248	.02	1.125	.0871	10.45	4.84	1391.6	1.00	27823	14.3	-0.00	.01
107.0	23377.3	171384	1656.0	162.6	158.7	.248	.00	1.128	.0875	10.50	4.85	1392.1	1.00	27822	14.3	-0.00	.00
108.0	23651.0	171380	1679.2	162.6	158.7	.248	.00	1.128	.0875	10.50	4.85	1392.6	1.00	27822	14.3	-0.00	.00
109.0	23924.7	171377	1702.4	162.6	158.6	.248	.01	1.128	.0875	10.50	4.84	1391.9	1.00	27822	14.3	-0.00	.00
110.0	24198.4	171373	1725.6	162.7	158.6	.248	.01	1.128	.0875	10.50	4.84	1390.0	1.00	27822	14.3	-0.00	.01
111.0	24472.2	171369	1748.7	162.7	158.5	.248	.01	1.128	.0875	10.50	4.84	1390.3	1.00	27821	14.3	-0.00	.01
ADVANCE THROTTLE SETTING TO 95.0 PERCENT IN 3.3 SEC.																	
112.0	24745.9	171365	1772.2	162.7	158.5	.248	.01	1.203	.0962	11.45	5.04	1449.2	1.07	29823	15.5	1.00	1.42
113.0	25019.4	171361	1797.6	162.7	158.4	.248	.01	1.231	.0995	11.80	5.60	1610.0	1.09	32049	16.4	-0.00	.63
114.0	25292.7	171356	1826.0	162.7	158.4	.248	.06	1.231	.0995	11.80	6.26	1797.5	1.10	34273	17.1	-0.00	.63
115.0	25565.7	171350	1857.5	162.7	158.3	.248	.00	1.199	.0957	11.40	6.88	1776.3	1.07	35236	17.3	-1.00	.63
116.0	25838.4	171344	1891.3	162.7	158.3	.248	.00	1.152	.0902	10.10	7.18	2062.0	1.03	35236	17.0	-0.00	.19
117.0	26111.1	171338	1926.0	162.7	158.2	.248	.01	1.132	.0880	10.55	7.30	2094.6	1.01	35235	16.8	-0.00	.07
118.0	26383.7	171332	1961.0	162.7	158.1	.248	.01	1.125	.0871	10.45	7.34	2107.3	1.00	35234	16.8	-0.00	.02
119.0	26656.3	171326	1996.2	162.7	158.0	.248	.01	1.125	.0871	10.45	7.35	2110.8	1.00	35234	16.8	-0.00	.01
ACCELERATE TO CLIMB SPEED OF 250.0 KNOTS																	
120.0	26928.9	171321	2031.3	162.8	158.0	.248	.15	1.093	.0837	10.05	7.28	2091.5	.97	35232	16.3	-0.50	-0.67
121.0	27201.8	171315	2065.5	162.9	158.1	.248	.44	1.054	.0795	9.55	6.98	2007.3	.94	35227	15.5	-0.50	-0.91
122.0	27475.4	171309	2097.8	163.0	158.3	.249	.84	1.015	.0755	9.05	6.45	1860.1	.90	35217	14.5	-0.50	-1.13
123.0	27750.3	171303	2127.2	164.0	158.9	.250	1.35	.975	.0717	8.55	5.71	1653.7	.87	35199	13.3	-0.50	-1.33
124.0	28026.9	171297	2152.7	164.3	159.8	.251	1.95	.938	.0683	8.07	4.78	1392.6	.85	35171	11.9	-0.25	-1.26
125.0	28305.9	171291	2173.5	165.3	161.0	.253	2.55	.914	.0665	7.82	3.75	1101.8	.84	35134	10.6	-0.25	-1.3
126.0	28587.8	171285	2189.3	165.0	162.6	.256	3.15	.899	.0648	7.57	2.69	800.1	.84	35086	9.3	-0.25	-1.31
127.0	28873.1	171280	2200.1	170.0	164.6	.259	3.22	1.044	.0785	9.42	1.68	504.1	1.00	35029	10.1	-0.25	-1.31
128.0	29161.8	171274	2208.6	171.9	166.4	.262	3.24	1.022	.0762	9.14	1.67	508.2	1.00	34973	9.8	-0.25	-1.33
129.0	29453.8	171266	2217.1	173.8	168.2	.265	3.25	1.001	.0742	8.87	1.65	508.1	1.00	34918	9.5	-0.23	-1.33
130.0	29749.0	171262	2225.5	175.7	170.1	.268	3.27	.980	.0722	8.61	1.64	508.2	1.00	34862	9.2	-0.23	-1.33
131.0	30047.5	171256	2234.0	177.7	171.9	.271	3.29	.960	.0703	8.35	1.62	508.2	1.00	34807	9.0	-0.23	-1.33
132.0	30349.3	171251	2242.5	179.6	173.8	.274	3.30	.940	.0685	8.10	1.60	508.1	1.00	34751	8.7	-0.23	-1.33
133.0	30654.3	171245	2250.9	181.6	175.7	.277	3.31	.921	.0667	7.86	1.58	508.1	1.00	34694	8.4	-0.23	-1.33
134.0	30962.7	171239	2259.4	183.5	177.5	.280	3.32	.903	.0651	7.62	1.57	508.1	1.00	34638	8.2	-0.23	-1.33
135.0	31274.4	171233	2267.9	185.5	179.4	.283	3.33	.885	.0636	7.40	1.55	508.0	1.00	34581	7.9	-0.23	-1.33
136.0	31589.5	171228	2276.2	187.5	181.3	.286	3.34	.867	.0621	7.17	1.53	508.0	1.00	34524	7.7	-0.23	-1.33
137.0	31907.5	171222	2284.8	189.5	183.2	.289	3.35	.850	.0607	6.95	1.52	508.0	1.00	34467	7.5	-0.23	-1.33
138.0	32229.6	171216	2293.3	191.5	185.1	.292	3.35	.833	.0594	6.74	1.50	508.0	1.00	34410	7.2	-0.23	-1.33
139.0	32554.7	171210	2301.7	193.4	187.0	.295	3.35	.817	.0581	6.54	1.48	507.9	1.00	34353	7.0	-0.16	-1.17
140.0	32883.1	171205	2310.2	195.4	188.9	.298	3.36	.801	.0569	6.33	1.47	508.0	1.00	34296	6.8	-0.23	-1.33
141.0	33214.9	171199	2318.7	197.4	190.8	.301	3.36	.786	.0558	6.14	1.46	508.3	1.00	34239	6.6	-0.23	-1.33
142.0	33550.1	171193	2327.1	199.4	192.7	.304	3.36	.771	.0547	5.95	1.44	508.2	1.00	34182	6.4	-0.16	-1.17
143.0	33888.6	171188	2335.6	201.4	194.6	.307	3.36	.757	.0536	5.76	1.43	508.3	1.00	34124	6.2	-0.23	-1.33
144.0	34230.5	171182	2344.1	203.4	196.5	.310	3.35	.743	.0527	5.59	1.41	508.3	1.00	34067	6.0	-0.16	-1.17

TAKEOFF CONTINUED

TIME (SEC)	DIST. (FEET)	WEIGHT (LBS)	ALT. (FEET)	TAS (KTS)	EAS (KTS)	MACH	ACCEL (FPS ²)	CL	CD	ALPHA (DEG)	GAMMA (DEG)	R/C (FPM)	LOAD FACT	THRUST (LBS)	FUS. ANG.	DALPH /DT	DTMTA /DT
145.0	34575.7	171176	2352.6	205.4	198.4	.313	3.35	.729	.0517	5.41	1.40	508.3	1.00	34010	5.8	-.23	-.25
FLAPS RETRACTED TO 2.0 DEG. IN 1.0 SEC.																	
146.0	34924.3	171171	2361.0	207.3	200.2	.316	3.36	.715	.0503	5.38	1.39	508.4	1.00	33953	5.8	1.17	1.16
147.0	35276.2	171165	2369.5	209.4	202.2	.319	3.53	.699	.0453	6.45	1.37	508.3	1.00	33894	6.8	-.16	-.17
148.0	35631.7	171159	2378.0	211.5	204.2	.322	3.53	.686	.0444	6.29	1.36	508.3	1.00	33834	6.6	-.16	-.17
149.0	35990.7	171154	2386.4	213.6	206.2	.326	3.53	.673	.0435	6.12	1.35	508.3	1.00	33774	6.5	-.16	-.17
150.0	36353.2	171148	2394.9	215.6	208.2	.329	3.53	.661	.0427	5.97	1.35	508.2	1.00	33714	6.3	-.16	-.17
FLAPS RETRACTED TO 0.0 DEG. IN .7 SEC.																	
151.0	36719.3	171143	2403.4	217.7	210.2	.332	3.53	.649	.0419	5.81	1.32	508.2	1.00	33654	6.1	-.16	-.17
152.0	37088.9	171137	2411.8	219.9	212.2	.335	3.67	.634	.0380	6.58	1.31	508.1	1.00	33592	6.9	-.16	-.17
153.0	37462.2	171131	2420.3	222.1	214.3	.339	3.67	.623	.0372	6.43	1.29	508.1	1.00	33530	6.7	-.16	-.17
154.0	37839.2	171126	2428.8	224.2	216.3	.342	3.67	.611	.0364	6.28	1.28	508.2	1.00	33467	6.6	-.16	-.17
155.0	38219.8	171120	2437.3	226.4	218.4	.345	3.67	.600	.0357	6.14	1.27	508.1	1.00	33405	6.4	-.16	-.17
156.0	38604.1	171115	2445.7	228.6	220.5	.349	3.67	.589	.0349	6.00	1.26	508.2	1.00	33342	6.3	-.16	-.17
157.0	38992.0	171109	2454.2	230.7	222.5	.352	3.67	.578	.0343	5.87	1.25	508.2	1.00	33279	6.1	-.16	-.17
158.0	39383.7	171104	2462.7	232.9	224.6	.355	3.66	.568	.0336	5.73	1.23	508.2	1.00	33217	6.0	-.16	-.17
159.0	39778.9	171098	2471.1	235.1	226.7	.359	3.66	.558	.0330	5.61	1.22	508.2	1.00	33155	5.8	-.08	-.09
160.0	40177.9	171093	2479.6	237.2	228.7	.362	3.66	.548	.0324	5.48	1.21	508.3	1.00	33092	5.7	-.16	-.17
161.0	40580.5	171087	2488.1	239.4	230.8	.365	3.65	.539	.0318	5.36	1.20	508.5	1.00	33030	5.6	-.16	-.17
162.0	40986.7	171082	2496.5	241.6	232.8	.368	3.65	.529	.0313	5.24	1.19	508.1	1.00	32968	5.4	-.16	-.17
163.0	41396.6	171076	2505.0	243.7	234.9	.372	3.64	.521	.0308	5.13	1.18	508.0	1.00	32905	5.3	-.08	-.09
164.0	41810.2	171071	2513.5	245.9	236.9	.375	3.63	.512	.0303	5.02	1.17	508.0	1.00	32843	5.2	-.08	-.09
165.0	42227.4	171065	2521.9	248.0	239.0	.378	3.62	.504	.0298	4.91	1.16	508.0	1.00	32781	5.1	-.08	-.09
EXECUTE PULLUP AT DADT = .13																	
166.0	42648.2	171060	2530.4	250.2	241.0	.382	3.59	.503	.0298	4.90	1.16	513.5	1.01	32720	5.1	.12	.17
167.0	43072.5	171054	2539.4	252.2	243.0	.385	3.43	.512	.0303	5.02	1.29	575.7	1.05	32659	5.3	.12	.33
168.0	43500.2	171049	2550.0	254.2	244.8	.38	3.19	.522	.0309	5.15	1.58	709.0	1.08	32602	5.7	.12	.48
169.0	43931.1	171044	2563.4	256.0	246.5	.391	2.87	.532	.0315	5.27	2.02	912.8	1.12	32550	6.3	.12	.63
170.0	44364.6	171038	2580.8	257.6	248.0	.393	2.47	.542	.0320	5.40	2.60	1185.1	1.16	32503	7.0	.12	.77
171.0	44808.3	171033	2603.3	258.9	249.2	.395	1.99	.552	.0326	5.52	3.33	1522.8	1.19	32464	7.9	.12	.91
172.0	45237.7	171027	2631.8	260.0	250.1	.397	1.52	.550	.0325	5.50	4.15	1904.4	1.19	32432	8.6	-.32	.45
173.0	45676.0	171022	2666.8	260.7	250.7	.398	1.05	.548	.0324	5.47	4.97	2286.8	1.20	32409	9.4	.12	.93
174.0	46114.9	171017	2708.1	261.2	251.0	.399	.60	.546	.0323	5.45	5.78	2668.7	1.20	32393	10.2	.12	.93
175.0	46553.7	171011	2755.7	261.4	251.0	.400	.15	.544	.0322	5.42	6.60	3043.1	1.19	32385	11.0	.12	.92
176.0	46991.9	171005	2809.1	261.4	250.8	.400	.01	.491	.0292	4.75	7.22	3331.1	1.08	32382	11.0	-.88	-.51
177.0	47429.8	171000	2865.5	261.4	250.6	.400	.01	.465	.0278	4.42	7.41	3417.6	1.02	32381	10.8	-.38	-.27
178.0	47867.7	170995	2922.7	261.4	250.4	.400	.01	.459	.0275	4.35	7.45	3436.9	1.01	32379	10.8	.12	.14
179.0	48305.5	170990	2980.0	261.4	250.2	.400	.01	.457	.0274	4.32	7.46	3442.1	1.00	32378	10.8	.12	.1
179.9	48699.5	170984	3031.7	261.4	250.0	.400	.01	.458	.0275	4.34	7.47	3443.3	1.00	32376	10.8	.12	.11

END OF TAKEOFF

** INPUTS TO LANDING - GROSS WT. =15000.0 WING AREA =1720.0 WING LOADING = 87.2
 ABAR= .35 CDGEAR= .026 OADT=1.0 DTABS= 0.0 OTDTMX= 7.0 ODPENG=3.0 FAFTR= .60 HAPR=35.0 HAPT= 0.0
 MSPOIL=10.0 IPWER= 0 ISPOIL= 1 PWRIOLE= .10 PWRMAX= 1.00 PWRMRG= .05 SINKTD= 3.0 TDELAY=1.0
 THEMAY= 20.0 TBRK= 0.0 IFLP= 99.0 TOFF= 3.0 TREV= 0.0 TSPL= 2.0 XMUBRK= .45 XLFMAX=1.15 XOIST=5000.0

LANDING
VKAPP = 130.0 GAMAPP = 3.00 RTSNK = 689.9 SINKTD = 3.00 XLFMAX = 1.15 ALPHM7 = 20.00
DELSPL = 0.00 DELFD = 40.00 ALPHA = 7.33 THRUST = 5825.1 IPOWER = 0 ISPOIL = 1
APPROACH AT THROTTLE SETTING = .459

TIME (SEC)	DIST. (FEET)	WEIGHT (LBS)	ALT. (FEET)	TAS (KTS)	EAS (KTS)	MACH NO.	ACCEL (FPS2)	CL	CD	ALPHA (DEG)	GAMMA (DEG)	R/C (FPM)	LOAD FACT	THRUST (LBS)	FUS. ANG.	THETA DOT
0.0	0.0	150000	35.0	130.0	129.9	.195	0.00	1.702	.2666	7.33	-3.00	689.9	1.00	17475	3.3	0.000
.5	109.7	150000	29.3	130.0	129.9	.195	0.00	1.702	.2666	7.33	-3.00	689.9	1.00	17475	3.3	0.000
1.0	219.4	150000	23.5	130.0	129.9	.195	0.00	1.702	.2666	7.33	-3.00	689.9	1.00	17475	3.3	0.000
1.5	329.1	150000	17.8	130.0	129.9	.195	0.00	1.702	.2666	7.33	-3.00	689.9	1.00	17475	3.3	0.000
** BEGIN FLARE AT 12.9 FEET																
1.9	422.6	150000	12.9	130.0	130.0	.197	-.24	1.702	.2666	7.33	-3.00	689.8	1.00	17475	3.3	0.000
2.0	444.6	150000	11.7	130.0	130.0	.197	-.35	1.717	.2687	7.53	-2.88	662.0	1.15	17475	3.7	3.222
2.1	466.5	150000	10.6	130.0	129.9	.197	-.43	1.721	.2692	7.58	-2.76	633.4	1.15	17475	3.8	1.741
2.2	488.5	150000	9.6	129.9	129.9	.197	-.50	1.721	.2692	7.54	-2.63	604.8	1.15	17475	4.0	1.237
2.3	510.4	149999	8.6	129.9	129.9	.197	-.58	1.725	.2698	7.63	-2.51	576.1	1.15	17475	4.1	1.754
2.4	532.3	149999	7.7	129.9	129.8	.197	-.64	1.725	.2698	7.63	-2.38	547.1	1.15	17475	4.3	1.249
2.5	554.2	149999	6.8	129.8	129.8	.196	-.71	1.725	.2698	7.63	-2.26	518.4	1.15	17475	4.4	1.243
2.6	576.2	149999	6.0	129.8	129.8	.196	-.79	1.729	.2703	7.68	-2.13	489.6	1.15	17475	4.6	1.759
2.7	598.1	149999	5.2	129.7	129.7	.196	-.86	1.729	.2703	7.68	-2.01	460.5	1.15	17475	4.7	1.252
2.8	620.0	149999	4.4	129.7	129.7	.196	-.92	1.729	.2703	7.68	-1.88	431.7	1.15	17475	4.8	1.244
2.9	641.9	149999	3.7	129.6	129.5	.196	-1.00	1.733	.2708	7.73	-1.76	402.9	1.15	17475	5.0	1.759
3.0	663.7	149998	3.1	129.6	129.6	.196	-1.06	1.733	.2708	7.73	-1.63	373.9	1.15	17475	5.1	1.250
3.1	685.6	149998	2.5	129.5	129.5	.196	-1.14	1.737	.2714	7.78	-1.51	345.0	1.15	17475	5.3	1.763
3.2	707.5	149998	1.9	129.4	129.4	.196	-1.20	1.737	.2719	7.83	-1.38	315.9	1.15	17475	5.4	1.253
3.3	729.3	149998	1.4	129.4	129.3	.196	-1.28	1.741	.2719	7.83	-1.25	287.0	1.15	17475	5.6	1.765
3.4	751.2	149998	1.0	129.3	129.3	.196	-1.34	1.741	.2719	7.83	-1.13	257.9	1.15	17475	5.7	1.254
3.5	773.0	149998	.6	129.2	129.2	.196	-1.42	1.745	.2724	7.88	-1.00	229.1	1.15	17475	5.9	1.765
3.6	794.8	149998	.2	129.1	129.1	.195	-1.48	1.745	.2724	7.88	-.88	200.1	1.15	17475	6.0	1.253
** TOUCHDOWN																
3.7	816.6	149997	0.0	129.0	129.0	.195	-1.56	1.749	.2730	7.93	0.00	180.0	0.00	17475	6.9	1.763
4.7	1033.8	149996	0.0	128.2	128.2	.194	-1.03	1.356	.2283	2.93	0.00	0.0	0.00	17498	1.9	-5.000
APPLY BRAKES AND/OR SPOILER AND/OR REVERSE THRUST - MUBRK = .450																
5.7	1248.7	149995	0.0	126.1	126.1	.191	-4.21	1.204	.2160	1.00	0.00	0.0	0.00	17525	0.0	0.000
6.7	1459.5	149993	0.0	123.5	123.5	.187	-4.46	1.204	.2160	1.00	0.00	0.0	0.00	17560	0.0	0.000
7.7	1665.1	149992	0.0	119.7	119.7	.182	-8.75	.925	.3086	1.00	0.00	0.0	0.00	17609	0.0	0.000
8.7	1862.3	149991	0.0	114.1	114.1	.174	-10.11	.894	.3195	1.00	0.00	0.0	0.00	13536	0.0	0.000
9.7	2049.3	149990	0.0	107.8	107.8	.164	-11.24	.894	.3195	1.00	0.00	0.0	0.00	8970	0.0	0.000
10.7	2225.0	149990	0.0	100.8	100.8	.154	-12.39	.894	.3195	1.00	0.00	0.0	0.00	4361	0.0	0.000
11.7	2388.3	149990	0.0	93.3	93.3	.142	-12.74	.894	.3195	1.00	0.00	0.0	0.00	3918	0.0	0.000
12.7	2539.0	149990	0.0	85.7	85.7	.131	-12.87	.894	.3195	1.00	0.00	0.0	0.00	3941	0.0	0.000
13.7	2676.7	149990	0.0	78.1	78.1	.119	-13.00	.894	.3195	1.00	0.00	0.0	0.00	3964	0.0	0.000
14.7	2801.5	149990	0.0	70.3	70.3	.108	-13.11	.894	.3195	1.00	0.00	0.0	0.00	3987	0.0	0.000
15.7	2913.1	149990	0.0	62.5	62.5	.096	-13.22	.894	.3195	1.00	0.00	0.0	0.00	4010	0.0	0.000
16.7	3011.5	149990	0.0	54.7	54.7	.084	-13.31	.894	.3195	1.00	0.00	0.0	0.00	4034	0.0	0.000
17.7	3096.6	149989	0.0	46.8	46.8	.072	-13.39	.894	.3195	1.00	0.00	0.0	0.00	4057	0.0	0.000
18.7	3168.3	149989	0.0	38.9	38.9	.060	-13.45	.894	.3195	1.00	0.00	0.0	0.00	4081	0.0	0.000
19.7	3226.5	149989	0.0	30.9	30.9	.048	-13.50	.894	.3195	1.00	0.00	0.0	0.00	4105	0.0	0.000
20.7	3271.3	149989	0.0	22.9	22.9	.036	-13.54	.894	.3195	1.00	0.00	0.0	0.00	4129	0.0	0.000
21.7	3302.5	149989	0.0	14.9	14.9	.024	-13.57	.894	.3195	1.00	0.00	0.0	0.00	4153	0.0	0.000
22.7	3320.1	149989	0.0	6.8	6.8	.012	-13.58	.894	.3195	1.00	0.00	0.0	0.00	4177	0.0	0.000
22.9	3324.4	149989	0.0	0.0	0.0	0.000	-13.58	.894	.3195	1.00	0.00	0.0	0.00	0	0.0	0.000

LANDING DISTANCE = 3324.4 FEET. FIELD LENGTH = 5540.7 FEET. ABAR = .342

A19NB06 * 7600 DAYFILE SUMMARY
 73/07/04* ** 1.1.6 BKY6 ** 73/06/18
 15.50.41* A19NBXX.P4.T50.CH70000.
 15.50.41.RUN76.S. COMPILING TEST1
 15.50.42. LCM 40000
 15.50.42. RUN76 COMPILE FL 044000
 15.50.42. TIME 000.065 SEC. BKY RUN76 LEVEL 5C
 15.50.42.ATTACH.A.BJEFF.
 15.50.42. LCM 100000
 15.50.43. LCM 140000
 15.50.43. LCM 200000
 15.50.43. LCM 240000
 15.50.44. FILE ATTACHED.
 15.50.44.ATTACH.B.SJEFF.
 15.50.44. FILE ATTACHED.
 15.50.44.COPY.A/RXP.IFM.B/RXB.IF.LGO.
 15.50.45.MAP.OFF.
 15.50.45.LINK.X.
 15.50.45. SCM 34000
 15.50.47.END TEST1
 15.50.47* ACCOUNTING INFORMATION.
 15.50.47* SCM KWS 38.98398
 15.50.47* LCM KWS 123.61856
 15.50.47* TRACKS 3
 15.50.47* I/O REQ. 326
 15.50.47* RMS CALLS 25
 15.50.47* LCM BLD. 9
 15.50.47* SWAPS 28
 15.50.47* CPU TIME 2.333 SECONDS.
 15.50.47* 73/07/04. 20 CJS.

BOWLES 029

- END OF SAMPLE CASE -

Program Listing

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TAKOFF      C
47      HEAD(S,AW2)
55      IF(INPC.EG. 1)PETLEN
63      ENP = XENG
64      SN = SWING
65      W = WGRSS
66      EYEW = EYEWLG
67      WU = UP
71      S(7) = WAPT
73      DU 7 I = 2,4
74      IF(XMPAR(I).NE. 0.0)XVPM(I) = 0.0
100      IF(XMVECT(I).NE. 0.0)XVVECT(I) = 0.0
104      7 CONTINUE

C
C      SET UP LOGIC CONTROL VARIABLES
C
106      NEG = 2
107      IPAGE = 0
110      KFLAG = 0
110      JJ1 = 1
111      JJ2 = 1
112      IUP = 1
113      IDOWN = 1
113      IFLY = 1
114      IFLAP = 2
115      KFLAP = 1
116      JROUTE = 1
116      IPGAER = 1
117      MPOWER = 2
120      MVECT = 1
120      IVECT = 2
121      135 = 1
122      IG = 0
123      AOUT = 0
123      ENPJ = ENP
125      ENPOT = ENP - 1.0

C
C      FIND GEAR DRAG IF DEFAULT OF CDGEAR=0.0 USED
C
126      IF(CDGEAR.FL. 0.0)CDGEAR = (U.0032/SN)*.***0.80
136      GMD = CDGEAR
137      IF(IDCN.NE. 9)GO TO 299
141      TEMP = 50.0 + DTASS
143      WG = WGRSS
144      WCS = W/SN

C
C      FIND STATIC THRUST/WEIGHT
C
146      CALL ENGINE(0.0,0.0,0.0,1.0,WFMENG)
152      TCA = ENP * THRUST / W

C
C      WRITE OUT PROGRAM INPUTS
C
155      WRITE(6,201)WAPT,TEMP
201      FORMAT(//, 3X * INPUTS TO TAKE OFF = ALTITUDE = ,F6.1,2X,14MTIEUP
          94RTURE = ,F5.1,7M DEG. C)

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TAKOFF
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TAKOFF
1106      113 CONTINUE
C
C      COMPUTE ALPHA DOT AND THETA DOT
C
1106      XDADT = (ALPHA - ALPHAJ)/T(3)
1111      DTHTDT = (THETA - THETAJ)/T(3)
1113      IF(NCOUNT .LT. 10)GO TO 1
1116      NCOUNT = 0
1116      VKTS = T(4) * 0.592087
1121      EAS = VKTS * SQRT(ANS(7))
1125      IF(IDCN .NE. 9)GO TO 1
1133      IF(IDCN .EQ. 9)
+WRITE(6,1002)T(2),T(5),W,ZERO,VKTS,EAS,EM,T(6),CL,CD,ALPHA,ZERO,
+ZERO,ZERO,TA,THETA,XDADT,DTHTDT
1212      IPAGE = IPAGE + 1
1214      IF(IPAGE .LT. NPAGE)GO TO 1
1216      IPAGE = 0
1216      IF(IDCN .EQ. 9)
+WRITE(6,996)
1227      IF(IDCN .EQ. 9)
+WRITE(6,1000)
GO TO 1
1240      120 VKTO = T(4) * 0.592087
1241      EASTO = VKTO * SURT(ANS(7))
1243      SRULL = T(5)
1247      IF(INDT .EQ. 1)ENP = ENPOUT
1251      IF(IDCN .EQ. 9)WRITE(6,1010)T(2),T(5),VKTO,EASTO
1260      1010 FORMAT(1X,17HLIFTOFF (TIME = ,F6.1,2X,7MOIST = ,F8.1,2X
+9,6MTAS = ,F7.1,1X,6MEAS = ,F7.1,1X))
1000 FORMAT(131F TIME DIST. HEIGHT ALT. TAS EAS MACH A
+R/C LCAD THRUST FUS. DAL
+GAMMA (FEET) (KTS) (KTS)
+CL CD ALPHA (DEG) (DEG) (DEG) (DEG) (DEG) (DEG) (DEG) (DEG)
+DTHTA,/,130M (SEC) (SEC) (SEC) (SEC) (SEC) (SEC) (SEC) (SEC)
+QND. (FPS2) /DT ,/)
1002 FORMAT(1X,F5.1,F9.1,F9.0,F9.1,F7.1,F6.1,F6.3,F7.2,F7.3,F7.4,2F7.2,
+9F8.1,F6.2,F9.0,F6.1,F7.2,F8.2)
C
C      END OF GROUND RULL - BEGIN AIRBORNE PORTION OF TAKEOFF
C
1303      VARG = PHARG*VEND
1305      THMAX = THFLY
C
C      FLAP, ANGLE AND POWER SCHEDULES SET UP FOR AIRBORNE PORTION
C
1306      WFLAP = WFLAP(2)
1310      VFLAP = VFLAP(2)
1311      HPWR = XWPR(2)
1313      VPR = XWPR(2)
1314      MVELT = XWVECT(2)
1316      VVECT = XWVECT(2)
1317      XLP = 1.0
C
C      AIRBORNE INTERMEDIATE VARIABLES
C      S(1) = NUMBER OF EQUATIONS
C      S(2) = TIME (SEC.)

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TAKOFF
1666 VJ = S(4)
1667 TJ5 = T(5)
1670 MJ = S(7)
1672 GO TO 22

C FIND VALUES AT 34 FT. (21-1015)
C
21 135 = 2
1672 535 = VVY(35.,TJ5,T(5),M. (7))
1673 V35 = VVY(35.,VJ,S(4),MJ,S(7))=SQRT(ANS(7))*0.592087
1703 IF(10CN .EQ. 4)
1722 WRITE(6,1015)S35,V35
1015 FORMAT(20H DISTANCE TO 35 FT.,F7.1,21H SCREEN SPEED(EAS) =,F6.1,
    10H KNOTS)
1743 22 IF(16 .EQ. 2)GO TO 25
1745 IF(16 .EQ. 1)GO TO 23

C GEAR RETRACTION (22-23)
C
1747 IF((S(7) - HAPT) .LT. HGN)GO TO 25
1752 TG = S(2)
1753 TGU = S(2) + DTGM
1755 IF(10CN .EQ. 4)
    WRITE(6,1025)TG,IGU
1025 FORMAT(14,27HGEAR RETRACTION STARTED AT ,F6.1,17H SEC,COMPLETE AT
    9,F6.1,4H SEC)
    IG = 1

1772 C GEAR DRAG INCREMENT REDUCED LINEARLY WITH TIME IN DTOR SECONDS
C
23 GMD = GMDGEAR*(1.0 - (S(2) - TG)/DTGM)
1773 IF(GMD .GE. 0.0)GO TO 25
1777 GMD = 0.0
2001 IG = 2
2002 CONTINUE
2003 IF(JMOUTE .EQ. 2)GO TO 39

C FLAP RETRACTION (25-16)
C
2005 IF(DELFD .EQ. 0.0)GO TO 16
2006 GO TO(10,15),MFLAP
2014 10 IF((S(7) - HAPT) .LT. MFLAP .OR. S(4)*SQRT(ANS(7))*0.542087 .LT.
    9 *FLAP)GO TO 16
    MFLAP = 2
    TIME = (DELFD - XDELFD(IFLAP))/DFLPT
    IF(10CN .EQ. 4)
    WRITE(6,1030)XDELFD(IFLAP),TIME
1030 FORMAT(14,19HFLAPS RETRACTED TO ,F4.1,9H DEG. IN ,F4.1,5H SEC.)
15 DELFD = DELFD - DFLPT*S(3)
    IF(DELFD .GT. XDELFD(IFLAP))GO TO 16
    DELFD = XDELFD(IFLAP)
    FLAP = 1
    JFLAP = IFLAP + 1
    MFLAP = XMFLAP(IFLAP)
    VFLAP = AVFLAP(IFLAP)

2061 C
2064
2070
2072
2074
2076

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TANOFF
C VECTORED THRUST ANGLE REDUCTION (14-56)
C
2101 10 CONTINUE
2102 IF(ANGLE .EQ. 0.)GO TO 56
2103 GO TO(50,55),MVECT
2110 50 IF((S(7)-MAPT) .LT. MVECT .ON. S(4)*SQR(ABS(7))=0.592087 .LT.
    9 MVECT)GO TO 56
2132 MVECT = 2
2132 TIME = (ANGLE - ANU(I ECT))/DTVECT
2136 IF(IDCN .EQ. 9)
    WRITE(6,1055)ANU(IVECT),TIME
1055 FORMAT(1A,3MVECTIONED THRUST ANGLE REDUCED TO ,F4.1,M DEG. IN ,
    94.1,5M SEC.)
2155 55 ANGLE = ANGLE - DTVECT*(3)
2160 IF(ANGLE .GT. ANU(IVECT))GO TO 56
2164 ANGLE = ANU(IVECT)
2166 MVECT = 1
2166 IVECT = IVECT + 1
2170 MVECT = ANU(IVECT)
2172 VVECT = ANU(IVECT)
C
C THROTTLE SETTING MANAGEMENT (50-59)
C
2175 50 CONTINUE
2175 GO TO(31,32,33),IPUMEN
2204 31 IF((S(7) - MAPT) .LT. MPUMEN .ON. S(4)*SQR(ABS(7))=0.592087 .LT.
    9 VPUMEN)GO TO 39
C
C DETERMINE POWER INCREASE OR DECREASE
C
2226 IF(PARSE1 - VPUMEN(MPUMEN)) ,39,35
C
C ADVANCE THROTTLE SETTING LOOP (34-35)
C
34 IPUMEN = 2
2233 TIME = 100.*(XPUMEN(MPUMEN) - PARSET)/DTPLUP
2233 SET = XPUMEN(MPUMEN)*100.
2237 IF(IDCN .EQ. 9)
2240 WRITE(6,1050)SET,TIME
1050 FORMAT(1X,2BADVANCE THROTTLE SETTING TO ,F6.1,12M PERCENT IN ,
    94.1,5M SEC.)
32 PARSET = PARSET + (DTPLUP/100.)*S(3)
2256 IF(PARSE1 .LT. XPUMEN(MPUMEN))GO TO 39
2262 PARSET = XPUMEN(MPUMEN)
2265 MPUMEN = MPUMEN + 1
2267 MPUMEN = MPUMEN + 1
2271 XPUMEN = XPUMEN(MPUMEN)
2273 VPUMEN = VPUMEN(MPUMEN)
2275 IPUMEN = 1
2276 GO TO 39
C
C RETARD THROTTLE SETTING LOOP (35-39)
C
35 IPUMEN = 3
2301 TIME = 100.*(PARSET - XPUMEN(MPUMEN))/DTPLDN
2301 SET = XPUMEN(MPUMEN)*100.
2305 IF(IDCN .EQ. 9)
2306

```


TAKOFF 996 FORMAT(,2,56PCANNOT ACCEI. AT INPUT K/C (HICL). TRY VALUE ,LT. L
 9AST K/C PRINTED)
 2674 WRITE(6,997)
 997 FORMAT(,1,38H*** ABNORMAL TERMINATION OF TAKOFF ***)
 2704 RETURN
 2704 END

SUBPROGRAM LENGTH

04066

FUNCTION ASSIGNMENTS

YYY - 000021

STATEMENT ASSIGNMENTS

1	- 000636	2	- 001350	3	- 001637	4	- 001623	5	- 000040	6	- 000064
7	- 000105	8	- 000513	9	- 002663	10	- 002015	15	- 002042	16	- 002102
21	- 001673	22	- 001744	23	- 001774	25	- 002004	26	- 001637	27	- 001517
28	- 001466	29	- 001514	31	- 002205	32	- 002257	33	- 002325	34	- 002232
35	- 002300	39	- 002346	41	- 001554	42	- 001563	43	- 001604	44	- 001620
50	- 002111	55	- 002156	56	- 002176	101	- 000746	102	- 001612	103	- 001003
105	- 000702	106	- 000666	110	- 001014	111	- 001051	112	- 001047	113	- 001107
120	- 001242	201	- 003064	202	- 003076	203	- 003114	204	- 003123	205	- 003141
206	- 003167	207	- 003212	208	- 003221	209	- 003230	210	- 003234	211	- 003240
212	- 003247	213	- 003256	299	- 000351	300	- 001373	996	- 003617	997	- 003630
998	- 003343	999	- 003270	1000	- 003364	1002	- 003421	1009	- 003317	1010	- 003351
1015	- 003476	1021	- 003305	1025	- 003507	1030	- 003522	1040	- 003446	1050	- 003545
1051	- 003557	1052	- 003574	1053	- 003600	1054	- 003607	1055	- 003532	1056	- 003463
1057	- 003334										

BLOCK NAMES AND LENGTHS

UNIV - 000030/01 AERU - 000020/02 EXCHNG - 000004/03 XROLL - 000041/04 XFLATE - 000072/05

VARIABLE ASSIGNMENTS

ALPHA	- 000010/02	ALPHAJ	- 004031	ALPHJ	- 004033	ANGLE	- 000005/02	ANS	- 003664	CD	- 000014/02
CDGEAR	- 003751	CL	- 00013/02	CY	- 000012/02	DADT	- 003773	DELFD	- 000006/02	DFLPDY	- 003752
DTABS	- 003753	DTFAIL	- 003772	DTCH	- 003754	DTHTDT	- 004043	DTPDNH	- 003755	DTPUP	- 003756
DTVECT	- 003757	EAS	- 004041	EASTO	- 004045	FM	- 000010/01	ENP	- 000021/01	ENPJ	- 004020
EMPOUT	- 004021	EVEW	- 000020/01	EYEWNG	- 003760	GAMIA	- 004065	GRCD	- 000016/02	HBS	- 000002/02
HAPT	- 003761	HFLAP	- 004047	HGR	- 003762	HJ	- 004060	HMAN	- 003763	HMAX	- 003774
MPOWER	- 04051	MVECT	- 004053	I	- 003776	TDOWN	- 004004	IFAST	- 000017/02	IPLAP	- 004006
IFLY	- 034005	IG	- 004016	IOUT	- 003764	TPAGE	- 003777	IPDWER	- 004011	IUP	- 000071/05
INVECT	- 004014	I35	- 004015	JJ1	- 004001	JJ2	- 004002	JROUTE	- 004010	K	- 000037/04
KENG	- 004000	KODE	- 004055	KEFLAP	- 004007	MOUT	- 004017	MPOWER	- 004012	MU	- 000003/04
MVECT	- 004013	KCOUNT	- 004030	NEG	- 000036/04	NPAGE	- 003775	PHARG	- 003766	PARSET	- 004025
OS	- 000011/02	PHO	- 000015/02	ROC	- 000044/05	FTCL	- 003747	S	- 000000/05	SA	- 004027
SET	- 004064	SHOLL	- 000000/03	SP	- 000015/01	S35	- 000001/03	T	- 000000/04	TA	- 000022/01
TEMP	- 004022	TG	- 004061	TGU	- 004062	THEMAX	- 000006/05	THETAJ	- 000006/05	THETAJ	- 004032
THRUST	- 000003/02	THTLY	- 003770	THTSCP	- 003771	TIME	- 004063	TJ5	- 004057	TOM	- 004024
T2J	- 004034	T4J	- 004035	TSJ	- 000003/03	UM	- 003765	VCL	- 000000/02	VEND	- 000001
VFLAP	- 004050	VJ	- 004056	VKTO	- 004044	VKTS	- 004040	VHARG	- 004046	VOUT	- 004037
VPDWER	- 004052	VH	- 000000	VVECT	- 004054	V35	- 000002/03	W	- 000006/01	WF	- 000007/01
WG	- 000023/01	WJ	- 004036	WUS	- 004023	XADT	- 004042	XDELFD	- 003674	XHFLAP	- 003701
XMPAP	- 003713	XHVECT	- 003737	XLF	- 000067/05	XLFMAX	- 000070/05	XNI	- 003732	XPOWER	- 003725

DERIV1

SUBROUTINE DERIV1

C SUBROUTINE DERIV1 COMPUTES THE ACCELERATION T(6) FOR THE GROUND ROLL

C

```

      REAL MU
      COMMON /UNIV/ NPC ,NSC ,IDC ,H ,ST ,R ,W ,
      1MF ,EM ,VMO ,ALPHLO,CLALPH,SM ,AP ,B ,
      2EVEN ,ENP ,TA ,MG ,MGS ,KWRITE,DLMCU
      3,KSIZE
      COMMON /AERO/ VEL,QS,MABS,THRUST,TVECT, ANGLE,DELFO,DELSPL,ALPHA,
      9CX,CY,CL,CD,MHD,GHCD,IFAST
      COMMON /XROLL/T(30),NEG,MU,NREV
      QS = 0.5*RH0*SM*T(4)*T(4)
      IF(QS .EQ. 0.)QS = 0.1
      IFAST = 1
      CALL AROOYN
      T(6) = (32.2/W)*(-W*W*W + QS*(CY*W - CX))
      T(7) = T(4)
      RETURN
      END
  
```

SUBPROGRAM LENGTH

00041

FUNCTION ASSIGNMENTS

STATEMENT ASSIGNMENTS

BLOCK NAMES AND LENGTHS

UNIV - 000030/01 AERO - 000020/02 XROLL - 000041/03

VARIABLE ASSIGNMENTS

CX - 000011/02 CY - 000012/02 IFAST - 000017/02 MU - 000037/03 QS - 000001/02 RHD - 000015/02
 SM - 000015/01 T - 000000/03 W - 000006/01

START OF CONSTANTS=000025 TEMPS=000031 INDIRECTS=000041

7600 COMPILATION -- RUN76 LEVEL 5C 73/07/05.

ROUTINE COMPILES IN 044000

DERIV3

```

SUBROUTINE DERIV3
C SUBROUTINE DERIV3 COMPUTES THE TIME DERIVATIVES FOR THE AIRBORNE
C PORTION OF THE TAKEOFF AND MANAGES THE FLIGHT PATH CONTROL.
C
COMMON /UNIV/ NPC ,NSC ,IDC ,M ,ST ,R ,M ,
IMF ,EM ,VMO ,EMMO ,ALPHLO,CLALPH,SM ,AR ,B ,
ZEYE ,ENP ,TA ,NG ,MGS ,KRITE,DLMC4
3,KSIZE
COMMON /AERO/ VEL,QS,MABS,THRUST,TVECT, ANGLE,DELFO,DELSPL,ALPHA,
9CX,CY,CL,CO,MHU,GRCD,IFAST
COMMON /AFLATE/ S(52),ROC,THEMAX,THETAF,XLF,XLFMAX,K
NER = 1
IFAST = 1
QS = 0.5*PMO*SM*MS(4)*S(4)
VKTS = S(4)*0.592087
C
C CONSTANT RATE OF CLIMB PORTION
C
IF(K.EQ.9)CALL CLIMB(ROC,S(5),VKTS,M=M)
IF(NER.NE.1)WRITE(6,666)ALPHA,ROC
666 FORMAT(IX,30H**ERROR IN CLIMB - ALPHA,ROC =,2F10.2)
26 IFAST = 0
CALL ARODYX
C
C CHECK FUSELAGE ANGLE. IF THETAF .GT. THEMAX, REDUCE ALPHA (261-262)
C
261 THETAF = S(5)*57.295 + ALPHA - EYEN
IF(THETAF .LE. THEMAX)GO TO 262
ALPHA = THEMAX + EYEN - S(5)*57.295
GO TO 26
C
C CHECK LOAD FACTOR. IF XLF .GT. XLFMAX, REDUCE ALPHA (262-263)
C
262 XLF = (QS*CY)/(M*COS(S(5)))
IF(XLF .LE. XLFMAX)GO TO 263
ALPHA = ALPHA - 0.05
GO TO 26
C
C CHECK ACCELERATION. IF S(8) .LT. 0.0, REDUCE ALPHA (263-30)
C
263 S(6) = (.52/2/M)*(-CX*QS - M*SIN(S(5)))
IF(S(8) .GE. 0.0)GO TO 30
ALPHA = ALPHA - 0.05
IF(ALPHA .LT. -2.0)GO TO 99
GO TO 26
30 CONTINUE
C
C COMPUTE S(9),S(10),S(11) (30-99)
C
S(9) = (.32/2/(M*S(4)))*(CY*QS - M*COS(S(5)))
IF(K.EQ.2.OH. K.EQ.4)S(8) = 0.0
IF(K.EQ.3.OH. K.EQ.4)S(9) = 0.0
S(10) = S(4) * COS(S(5))
S(11) = S(4) * SIN(S(5))
RETURN
99 WRITE(6,66)S(6)

```

DERIV3 66 F0PMAT(1X,40H*** UNABLE TO MAINTAIN ACCEL. .GE. 0.0, S(8) =,F9.5)
 141 K = 99
 142 RETURN
 143 END

SUBPROGRAM LENGTH

00223

FUNCTION ASSIGNMENTS

STATEMENT ASSIGNMENTS
 26 - 00031 30 - 00073 66 - 000164 94 - 000133 261 - 000033 262 - 000044
 263 - 00056 666 - 000152

BLOCK NAMES AND LENGTHS
 UNIV - 00030/01 AENG - 00020/02 XFLATE - 00072/03

VARIABLE ASSIGNMENTS
 ALPHA - 00010/02 CX - 00011/02 CY - 00012/02 EYEM - 00020/01 IFAST - 00017/02 K - 00071/03
 NER - 00021 GS - 00001/02 RMC - 00015/02 ROC - 00064/03 S - 00000/03 SM - 00015/01
 THEMEX - 00065/03 THETA - 00066/03 VKTS - 00022 W - 00006/01 XLF - 00067/03 XLFMAX - 00070/03

START OF CONSTANTS=000146 TEMPS=-000174 INDIRECTS=000216

7600 COMPILATION == RUN76 LEVEL 5C 73/07/05.

ROUTINE COMPILES IN 044100

CLIMB

```

SUBROUTINE CLIMB(RDC,GAMMA,VKTS,NEW)
C
C SUBROUTINE CLIMB FINDS THE REQUIRED ALPHA TO FLY AT THE CONSTANT
C RATE OF CLIMB RTCL, GIVEN THE THRUST AND VELOCITY. CHANGES IN FLIGHT
C PATH ANGLE ARE FAIRLY INSENSITIVE TO VARIATIONS IN ANGLE OF ATTACK.
C AS A RESULT, THE COMPUTED RATE OF CLIMB WILL DIFFER SOME (USUALLY LOW)
C THAN THE DESIRED VALUE RTCL.
C SUBROUTINE ZERJVM IS A ZERO-FINDER.
C

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```

      REAL NU
      COMMON /UNIV/ NPC ,NSC ,IDC ,H ,ST ,R ,W ,
      1MF ,EM ,VMO ,EMMO ,ALPHLO,CLALPH,SA ,AR ,B ,
      2ZEN ,ZEP ,TA ,AG ,AGS ,XAMPLTE,DLMCU
      3,KSIZE
      COMMON /AEC/ VFL,OS,MAHS,THRUST,IVECT, ANGLE,DELF,DELSPL,ALPHA,
      4CX,CY,CL,CD,MHO,GPCD,IFAST
      NEW = 1
      TOL = 0.01
      STEP = 1.0
      JX = 0
      JC = 0
      OS = 0.5*RDCL*VKTST*VKTST*2.8561*SM
      EMHOM = 959.
      40 IF(JX.EQ. 0)EMHOM1 = EMHOM
      IFAST = 0
      CALL ARDOYN
      ALPHA = ALPHA*.017453
      EMHOM = GS*(CY*COS(GAMMA) - CX*SIN(GAMMA)) - W
      IF(ABS(EMHOM) .LT. 0.0025)GO TO 60
      IF(JX.EQ. 2)GO TO 60
      CALL ZERJVM(EMHOM,EMHOM1,ALPHA,STEP,TOL,JC,JX)
      IF(JC.GT. 25)GO TO 65
      GO TO 40
      60 RETURN
      65 NEW = 9
      RETURN
      END

```

SUBPROGRAM LENGTH

00132

FUNCTION ASSIGNMENTS

STATEMENT ASSIGNMENTS

40 - C00021 60 - 000073 65 - 000074

BLOCK NAMES AND LENGTHS

UNIV - 000030/01 AEC - 000020/02

VARIABLE ASSIGNMENTS

ALPHA - 000010/02 ALPHX - 000131 CX - 000011/02 CY - 000012/02

IFAST - 000017/02 JC - 000124 JX - 000125 NU - 000127

STEP - 000124 SM - 000015/01 TUL - 000123 W - 000006/01

ERRM1 - 000150 ERROR - 000127
DS - 000001/02 RHO - 000015/02


```

LANDING
51 IF (IMPC .EQ. 1) RETURN
57 ENP = XENG
60 NER = 1
61 SW = SWING
62 WG = WGROSS
63 WOS = WG/SW
64 ALPHMX = THEMEX
C
C FIND GEAR DRAG IF DEFAULT OF CGEAR = 0.0 USED
C
66 IF (CGEAR .EQ. 0.0) CGEAR = (0.0032/SW)*WG**0.80
75 GKCD = CGEAR
76 IF (1) WRITE (.EQ. 1) GO TO 11
C
C WRITE OUT PROGRAM INPUTS
C
100 WRITE(6,7) WG, SW, WOS
7 FORMAT(1H1,1X,34H** INPUTS TO LANDING - GROSS WT. =,F8.1,14H WIN
96 AREA =,F6.1,17H WING LOADING =,F5.1)
116 WRITE(6,8) ABAR, CGEAR, DADT, DTABS, DTDTHX, DTPLNG, FAFTR, HAPT
8 FORMAT(1X,5HABAR=,F4.2,2X,7HCDGEAR=,F5.3,2X,5HDAOT=,F3.1,2X,
96HDTABS=,F4.1,2X,7HDTOTMX=,F4.1,2X,7HDTPLNG=,F3.1,2X,7HFAFTR=,
9F4.2,2X,5HHAPT=,F4.1,2X,5HWOS=,F6.1)
147 WRITE(6,9) MSPOIL, IPWR, ISPOIL, PWRIDL, PWRMAX, PWRMRG, SINKTD, TDELAY
9 FORMAT(1X,7HMSPOIL=,F4.1,2X,7HIPWR=,F4.1,2X,7HISPOIL=,F2.2X,
97HPWRIDL=,F4.2,2X,7HPWRMAX=,F5.2,2X,7HPWRMRG=,F4.2,2X,7HSINKTD=,
9F4.1,2X,7HDELAY=,F3.1)
176 WRITE(6,10) THEMEX, TBRK, TFLP, TOFF, TREV, TSPL, XMUBRK, XLFMAX, XOIST
10 FORMAT(1X,7HTHEMEX=,F5.1,2X,5HTBRK=,F4.1,2X,5HTFLP=,F5.1,2X,
95HTOFF=,F4.1,2X,5HTREV=,F4.1,2X,5HTSPL=,F5.1,2X,7HXMUBRK=,F4.2,2X,
97HXL FMAX=,F4.2,2X,6HADIST=,F6.1)
227 11 CONTINUE
C
C IF REQUESTED, FIND THE APPROACH SPEED VKAPP REQUIRED TO LAND IN THE
C DISTANCE XOIST FROM 35 FT. (11 - 100)
C VARIABLE JC COUNTS THE NUMBER OF TRIES TO FIND VKAPP (LIMIT OF 25)
C
227 IF (VKAPP .NE. 0.0) GO TO 100
230 F = 1.1
231 TOL = 0.25
233 JC = 0
234 JX = 0
236 VKAPP = 100.
237 FLD = XOIST
238 ERROR = 1.0
241 50 IF (JX .EQ. 0) ERRM1 = ERROR
244 CALL LAND(VKAPP, GAMAPP, XLFMAX, SINKTD, HAPT, ABAR, TDELAY, OIST)
254 ERROR = (FLD - OIST)/FLD
256 IF (JX .EQ. 2) GO TO 100
264 IF (ABS(ERROR) .LT. 0.005) GO TO 100
267 CALL ITRJVB(ERROR, ERRM1, VKAPP, F, TOL, JC, JX)
270 IF (JC .GT. 25) GO TO 97
275 GO TO 50
305 97 WRITE(6,96) VKAPP, GAMAPP, XLFMAX, SINKTD, HAPT, ABAR, TDELAY,
9ERROR, ERRM1, JC, JX
96 FORMAT(1X,24H*** FAILED TO FIND VKAPP,/,10X,45HVKAPP,GAMAPP,XLFMAX

```



```

LANDING
343 9,SINKTD,HAPP,ABAR,DELAY =,7F10.2/,10X,19HERROR,ERRM1,JC,JX =,
344 92F10.4,2I3)
345 MER = 99
      RETURN
      100 CONTINUE
C
C FIND THRUST AND ALPHA FOR STEADY STATE APPROACH, IF REQUESTED(100-200)
C
      HABS = 35.0
      IF(IZERO.EQ. 0)GO TO 200
      150 ALT = HAPT * HABS
      CALL ATMOS(ALT,DTABS,ANS)
      KENG = 1
      EN = VKAPP/ANS(4)
      VEL = VKAPP * 1.69
      OS = 0.5*ANS(3)*SW*VEL*VEL
      CALL ZERO(MER,EM,ALT,DTABS,KENG,PWRSET,QUESS)
      IF(MER.EQ. 1)GO TO 200
      156 WRITE(6,156)VKAPP,GAMAPP,ALT,DTABS,PWRSET,QUESS,ALPHMX,ENP,ST,M
      WRITE(5A,23H)*** FAILED IN ZERO-LAND,/,10X,31HVKAPP,GAMAPP,ALT,DTA
      156 FORMAT(5A,23H)*** FAILED IN ZERO-LAND,/,10X,23HQUESS,ALPHMX,ENP,ST,M =,5F10.2)
      985,PWRSET =,5F10.2/,10X,23HQUESS,ALPHMX,ENP,ST,M =,5F10.2)
      MER = 98
      RETURN
      200 CONTINUE
C
C ITERATION TO FIND PROPER FLARE INITIATION ALTITUDE(200-61)
C
C VARIABLE JC COUNTS THE NUMBER OF TRIES TO FIND HFLARE (LIMIT OF 25)
C
      HWRITE = 1
      IF(IWRITE.EQ. 3)NWRITE = 2
      TS = 0.0
      TIME = 0.0
      RTSNK = 101.4*VKAPP * SIN(GAMAPP*.0174533)
      TJ = THRUST
      DJ = DELSPL
      AJ = ALPHA
      PJ = PWRSET
      F = 1.25
      IF(HFLARE.NE. 0.0)F = STEP
      IF(HFLARE.EQ. 0.0)
      *HFLARE = ((VKAPP*1.69)**2) * ((GAMAPP/57.3)**2 - (SINKTD / (VKAPP
      1*1.69)**2) / (64.4 * (XLFMAX - 1.0)))
      IF(HFLARE.GT. 100.0 .OR. HFLARE.LT. 0.0)HFLARE = 25.0
      TOL = 0.1
      BU = 100.
      JC = 0
      JX = 0
      ERROR = 1.0
C
C LOOPING WITH HFLARE(40-60)
C
      40 IF (JX.EQ. 0) ERRM1 = ERROR
      525 THRUST = TJ
      530 DELSPL = DJ
      531 ALPHA = AJ
      533 PWRSET = PJ
      534

```

```

LANDING
536 W = WG
537 IF (NWRITE.EQ.2) WRITE(6,201) MFLARE,STEP,PWRSET,MSPOIL,SINKTD
201 FORMAT(1H1,/,3X,14MHFLARE,STEP,PWRSET,MSPOIL,SINKTD =,5F8.2)
564 IF (NWRITE.EQ.2) WRITE(6,1000)
576 CALL FLARE (MFLARE,PWRSET,MSPOIL,TS,TIME,NWRITE,ISPOIL,IPOWER)
C
C CHECK ACTUAL TOUCHDOWN RATE OF SINK AGAINST THAT DESIRED
C
606 ERROR = (RSTD - SINKTD) / SINKTD
610 IF (JX.EQ.2) GO TO 60
616 IF (ABS(ERROR).LT.0.025) GO TO 60
621 XPAST = MFLARE
622 YPAST = RSTD
C
C GUESS NEW MFLARE BASED ON ERROR(CALL ITRJVB)
C IF MFLARE IS LESS THAN 0.0 OR GREATER THAN 100.0 FT, EXIT PROGRAM
C
624 CALL ITRJVB(ERROR,ERRM1,MFLARE,F,TOL,JC,JX)
633 IF (JC.GT.25) GO TO 299
642 IF (MFLARE.GT.BU.OR.MFLARE.LE.0.) GO TO 299
652 GO TO 40
652 299 WRITE(6,298) MFLARE,RSTD,SINKTD,PWRSET,MSPOIL,IPOWER,ISPOIL
* ERROR,ERRM1,JC,JX
298 FORMAT(5X,24H*** FAILED IN FLARE-LAND,/,10X,48MHFLARE,RSTD,SINK
1TD,PWRSET,MSPOIL,IPOWER,ISPOIL = ,5F9.2,213/10X,19HERROR,ERRM1
1,JC,JX = ,2F7.4,213)
NER = 97
RETURN
711 60 THRUST = TJ
712 ALPHA = AJ
714 DELSPL = DJ
716 PWRSET = PJ
717 IF (JC.LT.1) GO TO 61
721 MFLARE = VY(MFLARE,XPAST,RSTD,YPAST,SINKTD)
723 *XLFMAX,ALPHA,DELSPL,DELFD,ALPHA,THRUST,IPOWER,ISPOIL,
9PWRSET
1001 FORMAT(1H1,2X,7MLANDING / 5X,7HVKAPP =,F5.1,3X,8HGAMAPP =,
1F5.2,3X,7HRTSNK =,F6.1,3X,8HSINKTD =,F5.2,3X,8HXLFMAX =,
9F5.2,3X,8HXLPMAX =,F5.2,/,5X,8HDELSPL =,F5.2,3X,7HDELFD =,F5.2,
93X,7HALPHA =,F5.2,3X,8HTHRUST =,F8.1,3X,8HIPOWER =,13.3X,
98HISPOIL =,13./,5X,30HAPPROACH AT THROTTLE SETTING =,F5.3,/)
1001 IF (NWRITE.GT.1) WRITE(6,1000)
C
C SET UP FOR PRINT OUT(61-160)
C
1013 IF (MFLARE.GE.HAPD) GO TO 161
1016 GO TO 162
1016 161 TIME = 0.0
1017 SAPP = 0.0
1017 OVER = MFLARE
1017 GO TO 160
1021 162 TIME = -0.5
1022 OVER = 0.0
1023 S(4) = VKAPP*1.69
1024 VKTS = VKAPP
1026

```

```

LANDING
1027 EAS = VKTS * SQRT(ANS(7))
1034 GAMMA = -GAMAPP
1035 S(8) = 0.0
1036 XLF = 1.0
1037 DTDT = 0.0
1040 CONST = (RTSNK/120.)/TAN(GAMAPP*.0174533)
1046 S(7) = HAPP + RTSNK/120.
1050 TS = -CONST
1055 163 S(7) = -RTSNK/120. * S(7)
1060 IF(S(7).GT. HFLARE)GO TO 164
1063 GO TO 165
1066 164 HABS = S(7)
1067 CALL ARODYN
1068 SAK7 = S(7)
1069 TS = TS + CONST
1070 TIME = TIME + 0.5
1073 IF(1WRITE.EQ. 1)GO TO 163
1101 S(8) = 0.0
1102 XLF = 1.0
1103 THRIST = ENP * THRUST
1105 THETAF = ALPHA - EYEW * GAMMA
1110 WRITE(6,1002)TIME,TS,WG,S(7),VKTS,EAS,EM,S(8),CL,CD,ALPHA,GAMMA,
9RTSNK,XLF,THRIST,THETAF,DTDT
GO TO 163
1160 165 XPART = (SAK7 - HFLARE)/(RTSNK/120.)
1164 TIME = TIME + XPART*0.5
1170 TS = TS + CONST*XPART
1172 160 IF(1WRITE.GT. 1)WRITE(6,899)HFLARE
1175 899 FORMAT(5X,18H** BEGIN FLARE AT ,F4.1,5H FEET)
W = WG
1211 C
1212 C
1213 C CALL TO FLARE WITH FINAL HFLARE VALUE
1223 CALL FLARE(HFLARE,PWRSET,MSPOIL,TS,TIME,1WRITE,ISPOIL,IPOWER)
IF(1WRITE.GT. 1)WRITE(6,996)
996 FORMAT(5X,12H** TOUCHDOWN)
VKTS = VKTD
EAS = VKTS*SQRT(ANS(7))
TS = STD
S(7) = 0.0
GAMMA = 0.0
XLF = 0.0
THRIST = ENP * THRUST
THETAF = ALPHA - EYEW
RTSNK = SINKTO * 60.
IF(1WRITE.GT. 1)WRITE(6,1002)S(2),TS,W,S(7),VKTS,EAS,EM,S(8),CL,
9CD,ALPHA,GAMMA,RTSNK,XLF,THRIST,THETAF,DTDT
1002 FORMAT(1X,F5.1,F9.0,F9.0,F7.1,F6.1,F6.3,F7.2,F7.2,
9F8.1,F6.2,F9.0,F6.1,F8.3)
1240 C
1241 C
1247 C
1250 C
1251 C
1252 C
1254 C
1256 C
1260 C
1342 C
1354 C
1371 C
1373 C CALL TO ROLL FOR GROUND ROLL OUT
C
C CALL ROLL(MODE,PWRSET,VKTD,STD,TIME,ABAR,TDDELAY,XHUBRK,TS,1WRITE)
IF(OVER.GT. 6.0)TS = TS - (HFLARE - HAPP)/TAN(GAMAPP*.0174533)
DLAND = TS/FAAFT
IF(1WRITE.GT. 1)WRITE(6,898)TS,DLAND,ABAR

```

LANDING

89A FORMAT(//3X,18LANDING DISTANCE =,F7.1,23M FEET. FIELD LENGTH =,
9F7.1,15M FEET. ABAR =,F6.3)
1000 FORMAT(13H TIME DIST. WEIGHT ALT. TAS EAS MACH A
9CCEL CL CD ALPHA GAMMA R/C LOAD THRUST FUS. TH
9ETA //,130H (SEC) (DEG) (FPM) FACT (LBS) ANG
9NU. (FPS2)
9. DOT
9. RETURN
9MO

1416
1417

SUBPROGRAM LENGTH

02271

FUNCTION ASSIGNMENTS

YYY - 000023

STATEMENT ASSIGNMENTS

S	- 000042	6	- 000060	7	- 001565	8	- 001601	9	- 001623	10	- 001644
11	- 000230	40	- 000526	50	- 000242	60	- 000714	61	- 000735	96	- 001672
97	- 000300	100	- 000346	150	- 000351	156	- 001714	160	- 001176	161	- 001617
162	- 001023	163	- 001056	164	- 001064	165	- 001165	200	- 000444	201	- 001744
298	- 001754	299	- 000553	898	- 002071	899	- 002043	996	- 002051	1000	- 002104
1001	- 001774	1002	- 002056								

BLOCK NAMES AND LENGTHS

UPV - 000030/01 AERO - 001020/02 XFLATE - 000072/03 XROLL - 000041/04 XLAND - 000007/05 LAND - 000003/06
PAL - 000005/07 MARGIN - 000003/08 TCHDOWN - 000003/11 ATMOSK - 000002/12

VARIABLE ASSIGNMENTS

ABAR	- 002213	AJ	- 002252	ALPHA	- 000010/02	ALPHMX	- 000002/06	ALT	- 002242	ANS	- 002203
BU	- 002254	CD	- 000014/02	CDGEAR	- 002214	CL	- 000013/02	CONST	- 002264	DADT	- 000004/07
DELFD	- 000006/02	DELSPL	- 000007/02	DIST	- 002241	OJ	- 002251	DLAND	- 002270	DTABS	- 000001/12
DTDT	- 000002/07	DTDTMX	- 000003/07	DTENG	- 000000/05	EAS	- 002262	EM	- 000010/01	ENP	- 000021/01
ERRM1	- 002240	ERROR	- 002237	EYEW	- 000020/01	F	- 002232	FAAFT	- 002215	FLD	- 002236
GAMAPP	- 000000/06	GAMMA	- 002263	GRCD	- 000016/02	HABS	- 000002/02	HAPP	- 002216	HAPT	- 000000/12
WFLARE	- 002230	ASPOIL	- 002217	IPOWER	- 002220	IREV	- 000002	ISPOIL	- 002221	IZERO	- 000001
JC	- 002234	JX	- 002235	KENG	- 002243	MODE	- 000000	NER	- 000003	NWRITE	- 002244
OVER	- 002260	PJ	- 002253	PWRIDL	- 000001/05	PWRMAX	- 000002/08	PWRMRG	- 000001/08	OS	- 000001/02
OUSS	- 002227	RSTD	- 000000/11	WTSNK	- 002247	S	- 000000/03	SAPP	- 002257	SINKTD	- 002222
ST	- 000004/01	STD	- 000002/11	STEP	- 002226	SW	- 0015/01	SXAT	- 002265	T	- 000000/04
TBRK	- 000002/05	TDELAY	- 002223	TFLP	- 000004/05	THEMAX	- 000005/03	THETAF	- 000066/03	THRIST	- 002266
THRUST	- 000003/02	TIME	- 002246	TJ	- 002250	TOFF	- 000006/05	TOL	- 002233	TREV	- 000005/05
TSPL	- 000003/05	TS	- 002245	VEL	- 000000/02	VKAPP	- 000001/06	VKTD	- 000001/11	VKTS	- 002220
W	- 000006/01	WG	- 000023/01	WOS	- 002231	XDIST	- 002224	XLF	- 000067/03	XLFMAX	- 000070/03
ALFMRG	- 000000/08	AMUBRK	- 002225	APART	- 002267	XPAST	- 002255	YPAST	- 002256		

START OF CONSTANTS-001556 TELPS--002141 INDIRECTS-002202

7600 COMPILATION -- RUN76 LEVEL 5C 73/07/04.

ROUTINE COMPILES IN 051500

FLARE

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SUBROUTINE FLARE(MFLARE,PMRSET,MSPOLL,T5,TIME,IWRITE,ISPOL,
9(POWER)
C
C SUBROUTINE FLARE COMPUTES THE FLARE MANUEVER BY RUNGE-KUTTA NUMERICAL
C INTEGRATION(CALL INTR). THE INTEGRATION STEP SIZE IS 0.1 SECONDS.
C THE INPUT VARIABLE MFLARE IS THE HEIGHT AT WHICH THE FLARE IS STARTED.
C
C THE VARIABLE DAGODA IS PROVIDED TO THE USER AS A MEANS TO ACCOUNT FOR
C A LOSS IN THE PITCH RATE CAPABILITY DUE TO NEGATIVE GROUND EFFECTS.
C DAGODA = 1.0 WOULD BE THE VALUE FOR OUT OF GROUND EFFECT, AND LESS THAN
C 1.0 FOR IN GROUND EFFECT. DAGODA MAY BE A FUNCTION OF WING HEIGHT/SPAN,
C TOTAL LIFT COEFFICIENT, CIRCULATION LIFT COEFF., ETC. AND SHOULD BE
C COMPUTED IN SUBROUTINE ARODYN AND PASSED THRU COMMON /EBFGRO/.
C THE USER MAY SIMPLY IGNORE DAGODA IF HE SO DESIRES.
C
C
C EXTERNAL DERIVZ
C DIMENSION ANS(8)
C COMMON /UNIV/ NPC ,NSC ,IDC ,H ,ST ,R ,W ,
C IMF ,EM ,VMO ,CMMD ,ALPHL9,CLALPH,SW ,AR ,B ,
C ZEYEW ,ENP ,TA ,WG ,WGS ,KWRITE,OLMC4
C 3,KSIZE
C COMMON /AERO/ VEL,QS,HABS,THRUST,TVECT, ANGLE,DELF,DELSPL,ALPHA,
C 9CX,CY,CL,CD,RHO,GRCD,IFAST
C COMMON /WFLATE/ S152,ROC,THEMAX,THEIAT,XLF,XLFMAX,K
C COMMON/LAND/ GAMAPP,VKAPP,ALPHMX
C COMMON/PAST/ ALPAST,XLPST,DTOT,DTOTMX,DAOT
C COMMON /EBFGRO/ DELJR,ETATRN,DAGODA
C COMMON/MARGIN/XLFMRG,PWRMRG,PWRMAX
C COMMON/TCMDWN/RSTD,VKTD,STD
C COMMON /ATMOSK/ HAPT,DTABS
C YYY(XNOW,XPAST,YNOW,YPAST,YANS)=XNOW-(YNOW-YANS)/((YPAST-YNOW)/
C *(XPAST-XNOW))
C
C INTEGRATION VARIABLES
C S(1) = NUMBER OF EQUATIONS
C S(2) = TIME (SEC.)
C S(3) = TIME INTERVAL, STEP SIZE (SEC.)
C S(4) = VELOCITY ALONG FLIGHT PATH (FT./SEC.)
C S(5) = FLIGHT PATH ANGLE (RAD.)
C S(6) = DISTANCE ALONG FLIGHT PATH (FT.)
C S(7) = ALTITUDE (FT.)
C S(8) = ACCELERATION ALONG FLIGHT PATH (FT./SEC.**2)
C S(9) = TIME RATE OF CHANGE OF FLIGHT PATH ANGLE (RAD./SEC.)
C S(10) = HORIZONTAL SPEED (FT./SEC.)
C S(11) = RATE OF CLIMB (FT./SEC.)
C N = 4
C IMODE = 1
C JMODE = 1
C MRROUTE = 1
C DAGODA = 1.0
C W = WG
C
C 31
C 32
C 33
C 34
C 35
C
C INITIALIZATION FOR INTEGRATION LOOP(109-108)
C
C S(1) = 4
C S(2) = TIME

```


FLARE

```

276     SIPS/ = S(11)
277     IF(IWRITE.EQ. 1) GO TO 107
278     IF(XLF.GT. XLFMAX)XLF = XLFMAX
301     VKTS = S(4)/1.69
304     EAS = VKTS * SORT(ANS(7))
306     GAMMA = S(5) * 57.3
313     RTSNK = -60. * S(11)
314     THETA = ALPHA + EYEW * S(5)*57.3
316     THRIST = ENP + THRUST
322     IF(S(7).LT. 0.001)S(7) = 0.10
324     WRITE(6,1002)S(2),TS,W,S(7),VKTS,EAS,EM,S(8),CL,CD,ALPHA,GAMMA,
332     *RTSNK,XLF,THRIST,THETA,OTDT
1002  FORMAT(1X,F5.1,F9.1,F9.0,F9.1,F7.1,F6.1,F6.3,F7.2,F7.3,F7.4,F7.2,
      9F8.1,F6.2,F9.0,F5.1,F8.2)
412     107 CONTINUE
      C
      C SPOILER RETRACTION(107-89)
      C
412     IF(ISOIL.EQ. 0 .OR. DELSPL.EQ. 0.0)GO TO 89
420     IF((PWRMAX - PWRSET) .LE. PWRMRG)GO TO 80
423     IF(HABS.GT. HSPoil)GO TO 89
427     IF(ABS(XLFMAX - XLF) .LE. XLFMRG)GO TO 89
433     80 DELSPL = DELSPL - 2.5
435     IF(JNODE.EQ. 1 .AND. IWRITE.GT. 1)WRITE(6,91)HABS
      86  FORMAT(5X,22HSPOLERS RETRACTED AT ,F4.1,14H FEET ALTITUDE)
      JNODE = 2
456     IF(DELSPL.LT. 0.0)DELSPL = 0.0
457     CALL DERIV2
461     IF(DELSPL.EQ. 0.0)GO TO 89
462     IF(ABS(XLFMAX - XLF) .LE. XLFMRG)GO TO 89
467     GO TO 80
473     89 CONTINUE
      C
      C THRUST MODULATION(89-99)
      C
474     IF(POWER.EQ. 0)GO TO 99
476     IF(XLF.GE. XLFST)GO TO 99
501     PWRSET = PWRSET + 0.01
502     IF(JNODE.EQ. 1 .AND. IWRITE.GT. 1)WRITE(6,91)
91  FORMAT(5X,50HTHRUST MODULATION REQUIRED TO MAINTAIN LOAD FACTOR )
521     INODE = 2
522     IF(PWRSET.GT. PWRMAX)PWRSET = PWRMAX
      C
      C CALL ENGINE IF POWER SETTING CHANGED (KENG = 2) AND TRY TO MAINTAIN
      C LOAD FACTOR.
      C
525     KENG = 2
526     CALL ENGINE(INAL,DTABS,EM,PWRSET,MF,KENG)
533     IF(PWRSET.EQ. PWRMAX)GO TO 99
541     CALL DERIV2
542     IF(XLF.GE. XLFMAX)GO TO 99
550     GO TO 90
551     99 CONTINUE
      C
      C GO TO 108
      C
      C FIND RATE OF SINK AT TOUCHDOWN.

```

FLARE

```

C
552 300 RSTD =-YYY(S(11),S11PST,S(7),S7PAST*0.0)
563 VKTD = S(4)/1.69
565 STD = Y5
566 TIME = S(2)
567 RETURN
570 301 RSTD = 0.
571 RETURN
572 END

```

SUBPROGRAM LENGTH

00720

FUNCTION ASSIGNMENTS

YYY - 000021

STATEMENT ASSIGNMENTS

70	-	000233	80	-	000434	86	-	000624	89	-	000475	90	-	000477	91	-	000634
99	-	000552	107	-	000413	108	-	000206	109	-	000055	300	-	000553	301	-	000571
1002	-	000611															

BLOCK NAMES AND LENGTHS

UNIV	-	000030/01	AERO	-	000072/03	LAND	-	000003/04	PAST	-	000005/05	EBFGRD	-	000003/06
MARGIN	-	000003/07	TCDOWN	-	000003/08	ATMOSX	-	000002/11						

VARIABLE ASSIGNMENTS

ALPAST	-	000000/05	ALPHA	-	000010/02	ANS	-	000673	CD	-	000014/02	CL	-	000013/02	DADT	-	000004/05
DAGODA	-	000002/06	DELSPL	-	000007/02	DTABS	-	000001/11	DTDT	-	000002/05	EAS	-	000710	EM	-	000010/01
EMP	-	000021/01	EYEW	-	000020/01	GAMAPP	-	000000/04	GAMMA	-	000711	HABS	-	000002/02	MALT	-	000714
HAPT	-	000000/11	INODE	-	000704	POWER	-	000001	ISPOIL	-	000000	JNODE	-	000705	KENG	-	000717
MROUTE	-	000706	N	-	000703	PWRMAX	-	000002/07	PWRMRG	-	000001/07	RHO	-	000015/02	RSTD	-	000000/08
RTSNK	-	000712	S	-	000000/03	STD	-	000002/08	S11PST	-	000716	S7PAST	-	000715	TMETAF	-	000066/03
THRIST	-	000713	THRUST	-	000003/02	VEL	-	000000/02	VKAPP	-	000001/04	VKTD	-	000001/08	VKTS	-	000707
W	-	000006/01	WF	-	000007/01	WG	-	000023/01	XLF	-	000067/03	XLPHAX	-	000070/03	XLFMRG	-	000000/07
XLFPST	-	000001/05															

START OF CONSTANTS-000575 TEMPS--000647 INDIRECTS-000671

7600 COMPILATION -- RUN76 LEVEL 5C 73/07/04.

ROUTINE COMPILES IN 045700

ROLL

```

C      SUBROUTINE ROLL(MODE,PWRSET,VKTD,STD,TMTD,ABAR,TDELAY,XMUBRK,TS,
C      9)WRITE)
C      SUBROUTINE ROLL COMPUTES THE GROUND ROLL OF THE LANDING MANEUVER.
C      VKTD = INITIAL SPEED, STD = INITIAL DISTANCE, TMTD = INITIAL TIME.
C
C      EXTERNAL DERIV4
C      REAL MU
C      COMMON /UNIV/ NPC      *NSC      *IDC      *H      *ST      *R      *W      *
C      1WF      *EM      *VM0      *EMM0      *ALPHL0*CLALPH*SM      *AR      *B      *
C      2EYEW      *ENP      *TA      *WG      *WGS      *KWRITE*DLMC4
C      3*KSIZ
C      COMMON /AERO/ VEL*QS*HABS*THRUST*VTECT, ANGLE*DELF*DELSPL*ALPHA*
C      9CX*CY*CL*CD*RH0*GRCD*IFAST
C      COMMON /XROLL/ T(30)*NEQ*NU*NREV
C      COMMON /ALAND/ DTPENG,PWRIDL,TBRK,TSPL,TFLP,TREV,TOFF
C      COMMON /ATMOSX/ HAPT,DTABS
C      DIMENSION ANS(8)
C      SXX7 = 0.0
C
C      ENGINE THROTTLING SET UP
C
C      DTPUP = (1.0 - PWRSET)/DTPENG
C      DTPDWN = (PWRSET - PWRIDL)/DTPENG
C      PJ = PWRSET
C      TJUN = TDELAY + TOFF
C      TJREV = TDELAY + IQEV
C      NREV = 0
C      ROUTE = 1
C      ROUT1 = 1
C      ROUT2 = 1
C      ROUT3 = 1
C      ROUT4 = 1
C      ROUTJ = 1
C
C      MODE = 1 - RUNGE-KUTTA INTEGRATION OF GROUND ROLL.
C      MODE = 2 - LANDING DISTANCE CALCULATED ASSUMING AN AVERAGE DECELERATION.
C
C      GO TO (100,200),MODE
C      200 STOP = (1.0/(64.4*ABAR))*(VKTD*1.69)**2 + 1.69*VKTD*TDELAY
C      TS = STD + STOP
C      RETURN
C
C      INTEGRATION VARIABLES
C      T(1) = NUMBER OF EQUATIONS
C      T(2) = TIME (SEC.)
C      T(3) = TIME INTERVAL* STEP SIZE (SEC.)
C      T(4) = VELOCITY (FT./SEC.)
C      T(5) = DISTANCE (FT.)
C      T(6) = ACCELERATION (FT./SEC.**2)
C
C      100 NEQ = 2
C      T(1) = 2
C      T(2) = 0.0
C      T(3) = 0.1
C      T(4) = VKTD*1.69

```


	C	CHANGES TO THROTTLE SETTING (140-150)
215	C	140 IF(IROUT4.EQ. 2)GO TO 150
217		IF(IREV.EQ. 1)GO TO 145
	C	THROTTLE DOWN TO IDLL (140-145)
221	C	IF(I(2).LT.(TDELAY + TOFF))GO TO 150
225		PWRSET = PJ - DTPDN*(I(2) - TJDN)
230		IF(PWRSET.GT. PWRIDL)GO TO 150
234		PWRSET = PWRIDL
236		IROUT4 = 2
235		GO TO 150
	C	ADVANCE THROTTLE FOR REVERSE THRUST (145-150)
236	C	145 IF(I(2).LT.(TDELAY + TREV))GO TO 150
242		NREV = 1
243		PWRSET = PJ + DTPUP*(I(2) - TJREV)
247		IF(PWRSET.LT. 1.0)GO TO 150
251		PWRSET = 1.0
252		IROUT4 = 2
253		150 CALL INTMT(NEQ,2,1.,1.,1.,1.,1., DERIV4)
265		T5 = T5 + T(3)*T(4)
270		ACCEL = ACCEL + T(b)
	C	CALL ENGINE WITH PWRSET(KENG=2) AND GET THRUST AND FUEL FLOW.
272	C	KENG = 2
273		CALL ENGINE(MAPT,DTABS,EM,PWRSET,WF,KENG)
303		W = W - WF*ENPOT(3)/3600.
	C	LIMIT ON GROUND ROLL OF 60. SECONDS.
307	C	IF(I(2).GT. 60.0) GO TO 199
317		IF(I(4).LT. 1.0)GO TO 190
321		IF(IMWRITE.EQ. 1)GO TO 101
323		IF(INCOUNT.LT. 10)GO TO 101
326		NCOUNT = 0
326		TIME = TIMTD + T(2)
327		VKTS = T(4)/1.69
332		EAS = VKTS * SORT(ANS(7))
337		THETA_F = ALPHA - EYEW
340		THRIST = THRUST * ENP
343		WRITE(6,1002)TIME,T5,W,ZERO,VKTS,EAS,EM,T(6),CL,CD,ALPHA,ZERO
		9,ZERO,ZERO,THRIST,THETA_F,DYD
		1002 FORMAT(1X,F5.1,F9.1,F9.0,F9.1,F7.1,F6.1,F6.3,F7.2,F7.3,F7.4,2F7.2,
		9F8.1,F6.2,F9.0,F6.1,F8.3)
421		GO TO 101
421		190 STD = T5
422		TIME = TIME + 0.2
424		WRITE(6,1002)TIME,T5,W,ZERO,ZERO,ZERO,I(6),CL,CD,ALPHA,ZERO,
		9ZERO,ZERO,ZERO,ZERO
	C	COMPUTE AVERAGE DECELERATION ABAR FOR MODE = 1
	C	

```

ROLL 473      ABAR = -(ACCEL/(T(2)*10.0))/32.2
      502      RETURN
      503      199 WRITE(6,198)
      513      198 FORMAT(5X,23H*** FAILED IN ROLL-LAND)
      513      RETURN
      513      END

```

SUBPROGRAM LENGTH

00644

FUNCTION ASSIGNMENTS

STATEMENT ASSIGNMENTS	
100 - 00052	101 - 000132
140 - 000216	145 - 000254
200 - 000041	1002 - 000550

BLOCK NAMES AND LENGTHS

UNIV - 000030/01	AERO - 000020/02	XROLL - 000041/03	XLAND - 000007/04	ATMOSK - 000002/05
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VARIABLE ASSIGNMENTS

ACCEL - 000632	ALPHA - 000010/02	ANS - 000604	CD - 000014/02	CL - 000013/02	DELFD - 000006/02
DELSPL - 00007/02	DTABS - 000001/05	DTDT - 000634	DTPDWN - 000516	DTPENG - 000000/04	UTPUP - 000615
EAS - 000641	EM - 000010/01	ENP - 000021/01	EYEW - 000020/01	HABS - 000002/02	HAPT - 000000/05
IREV - 000635	IROUTE - 000622	IROUTJ - 000627	IROUT1 - 000623	IROUT2 - 000624	IROUT3 - 000625
IROUT4 - 000626	IWRITE - 000003	KENG - 000636	MU - 000037/03	NCOUNT - 000633	NEO - 000036/03
MREV - 000040/03	PJ - 000617	PWRIDL - 000001/04	RHO - 000015/02	STOP - 000630	SXX7 - 000614
T - 000000/03	TBRK - 000002/04	TDELAY - 000000	TFLP - 000004/04	THETAF - 000642	THRIST - 000643
THRUST - 000003/02	TIME - 000637	TJDNW - 000620	TJREV - 000621	TOFF - 000006/04	TREV - 000005/04
TSPL - 000003/04	TS - 000002	VKTS - 000640	W - 000006/01	WF - 000007/01	XNUBRK - 000001
ZERO - 000631					

START OF CONSTANTS-000516 TEMPS--000572 INDIRECTS-000603

7500 COMPILATION -- RUN76 LEVEL 5C 73/07/04.

ROUTINE COMPILES IN 045400

```

DERIV4
C
C SUBROUTINE DERIV4 COMPUTES THE DERIVATIVES FOR INTEGRATION IN ROLL.
C
      REAL MU
      COMMON /UNIV/ NPC ,NSC ,IDC ,H ,ST ,R ,W ,
      1WF ,EM ,VM0 ,ALPH0,CLAPH,SM ,AR ,B ,
      2EYEW ,EMP ,TA ,WG ,WGS ,WRITE,OLMC4
      3KSIZE
      COMMON /AERO/ VEL,OS,HABS,THRUST,TVECT, ANGLE,DELF,DELSPL,ALPHA,
      9CX,CY,CL,CD,RHO,GRCD,IFAST
      COMMON /XROLL/ T(30),NEQ,MU,NREV
      OS = 0.5*RM0*SM*T(4)*T(4)
      IF (OS .EQ. 0.) OS = 0.1
4
C
C IF USING REVERSE THRUST (NREV .EQ. 1) CALL SUBROUTINE REVRSE TO
C OBTAIN CX AND CY IN THE REVERSE THRUST MODE.
C
      IF (NREV .EQ. 0) CALL ARODYN
      IF (NREV .EQ. 1) CALL REVRSE
      T(6) = (32.2/W)*(-W*MU + OS*(CY*MU - CX))
      T(7) = T(4)
      RETURN
      END
25

```

SUBPROGRAM LENGTH

00044

FUNCTION ASSIGNMENTS

STATEMENT ASSIGNMENTS

BLOCK NAMES AND LENGTHS

UNIV	- 000030/01	AERO	- 000020/02	XROLL	- 000041/03	OS	- 000040/03	NREV	- 000037/03	RHO	- 000015/02
VARIABLE ASSIGNMENTS											
CX	- 000011/02	CY	- 000012/02	MU	- 000037/03	OS	- 000040/03	NREV	- 000037/03	RHO	- 000015/02
SW	- 000015/01	T	- 000000/03	W	- 000006/01						
START OF CONSTANTS-000030			TEMPS--000034		INDIRECTS-000044						
7600 COMPILATION -- RUN76 LEVEL 5C			73/07/04.								
ROUTINE COMPILES IN 044000											

```

LAND1
C      SUBROUTINE LAND1(VKAPP,GAMAPP,XLFMAX,SINKTD,HAPP,ABAR,TOELAY,DIST)
C      SUBROUTINE LAND1 IS USED IN FINDING THE REQUIRED APPROACH SPEED IN
C      SUBROUTINE LANDING. IT CALCULATES THE LANDING DISTANCE ASSUMING A
C      CONSTANT SPEED AND LOAD FACTOR FLARE.
C      VKAPP = SPEED(KNOTS)
C      XLFMAX = MAX. LOAD FACTOR
C      ABAR = AVERAGE DECELERATION(G'S)
C      TDELAY = TIME DELAY (SEC.)
C      GAMAPP = GAMAPP/57.3
C      VAPP = VKAPP * 1.69
C      GAMTD = SINKTD/VAPP
C      R = (VAPP*VAPP)/(32.2*(XLFMAX - 1.0))
C      MFLAR = VAPP*VAPP*(GAMX*GAMX - GAMTD*GAMTD)/(64.4*(XLFMAX-1.0))
C      IF(MFLAR .LT. HAPP)GO TO 20
C      DLGL = 0.0
C      DLTR = R*(SORT((2.*HAPP/R)* GAMTD*GAMTD) - GAMTD)
C      GO TO 25
C      20 DLGL = HAPP/TAN(GAMX)
C      25 DLTR = ((R*GAMX)/2.)*((1.0 - GAMTD/GAMX)**2)
C      25 DOELAY = VAPP*TOELAY
C      DGRND = (1.0/(64.4 * ABAR))*VAPP*VAPP
C      DIST = DLGL + DLTR + DOELAY + DGRND
C      RETURN
C      END

SUBPROGRAM LENGTH
00144

FUNCTION ASSIGNMENTS
STATEMENT ASSIGNMENTS
20 - 000050 25 - 000065

BLOCK NAMES AND LENGTHS
VARIABLE ASSIGNMENTS
DOELAY - 000142 DGRND - 000143 DIST - 000001 DLGL - 000140
GAMX - 000133 MFLAR - 000137 R - 000136 TDFLAY - 000000
START OF CONSTANTS-000101 TEMPS--000110 INDIRECTS-000133
7600 COMPILATION -- RUN76 LEVEL 5C 73/07/04.
ROUTINE COMPILES IN 044000

```

```

SUBROUTINE ZERO(NER,EN,ALT,DATABS,KENG,PWRSET,QUESS)
C SUBROUTINE ZERO COMPUTES THE REQUIRED VALUES OF THRUST PER ENGINE AND
C ANGLE OF ATTACK FOR ZERO ACCELERATION ALONG AND NORMAL TO THE FLIGHT
C PATH. DV/DOT AND DG/DOT, RESPECTIVELY. THE SUBROUTINE CALLS ENGINE
C WITH KENG = 1 WITH A VALUE OF THRUST TO OBTAIN THE POWER SETTING.
C THE OUTER LOOP VARIES THE THRUST, WITH TWO INNER LOOPS VARYING ALPHA
C FROM ALPHA TO -ALPHMX. FOR A FIXED VALUE OF THRUST (OUTER LOOP),
C SUBROUTINES ODVT(ACCELERATION ALONG FLIGHT PATH), AND ODGT(ACCELERATION
C NORMAL TO FLIGHT PATH), ARE CALLED WITH THE VALUES OF ALPHA (INNER
C LOOP). THESE TWO FUNCTION SUBROUTINES CALL ARODYN. SUBROUTINES
C ITRJVB AND ZERXO ARE BOTH ZERO-FINDERS.
C
      EXTERNAL DVDT,DGDT
      COMMON /UNIV/ NPC ,NSC ,IDC ,M ,ST ,P ,W ,
      1WF ,EM ,VMO ,ENMO ,ALPHL0,CLALPH,SW ,AR ,B ,
      2REVE ,EMP ,TA ,WG ,NGS ,KWRITE,DLMC4
      3,KSIZE
      COMMON /AERO/ VEL,QS,HABS,THRUST,TVECT, ANGLE,DELF,D,DELSPL,ALPHA,
      9CA,CY,CL,CD,NQD,GRCDD,IFAST
      COMMON/LAND/ GAMAPP,VKAPP,ALPHMX
      EM = EN
      NER = 1
      EPS = 0.001
      ALPHMN = - ALPHMX
C
C FIRST QUESS AT THRUST
C
      TFIRST = (ST/ENP) * QUESS
      1 THRUST = TFIRST
      F = 0.95
      TOL = ST/(ENP*1000.)
      IF(TOL .LT. 5.0)TOL = 5.0
      BU = W/ENP
      BL = W / 100.
      JC = 0
      JA = 0
      ERROR = 999.
C
C OUTER LOOP WITH THRUST (2-10)
C
      2 IF (JA .EQ. 0) ERRN1 = ERROR
C
      CALL ENGINE
      CALL ENGINE(ALT,DATABS,EM,PWRSET,WF,KENG)
C
C FIND VALUE OF THRUST SUCH THAT DV/DOT IS NEGATIVE AT ALPHA = ALPHMX,
C WITH A REDUCTION IN ALPHA RESULTING IN LESS DRAG. DV/DOT WILL CHANGE
C SIGN(I.E. A BOUNDED INTERVAL IN WHICH DV/DT = 0.0 WILL BE FOUND).
C
      ALPHUP = ALPHMX
      XUP = DVDT(ALPHUP)
      IF (XUP .LT. 0.-0) GO TO 3
      7 TFIRST = TFIRST/1.25
      IF (TFIRST .LT. BL) GO TO 99

```



```

ZERO 63      GO TO 1
C
C SEARCH FOR DV/DT = 0.0 FROM ALPHMX TO -ALPHMX (3-4)
C
64 3 ALPXLO = ALPXUP - 2.0
66 IF (ALPXLO .LT. ALPHMX) GO TO 98
71 XLO = DVTI(ALPXLO)
C
C CHECK TO SEE IF DV/DT = 0.0 IS BOUNDED.
C
72 IF (XLO * XUP .LE. 0.0) GO TO 4
100 ALPXUP = ALPXLO
101 XUP = XLO
103 GO TO 3
C
C ONCE ALP... INTERVAL FOR DV/DT = 0.0 IS BOUNDED, CALL ZEROX TO FIND
C ALPHA1, THE VALUE OF ALPHA FOR DV/DT = 0.0.
C
103 4 ALPHA1 = ZEROX(ALPXLO,ALPXUP,DVDT,EPS)
C
C SEARCH FOR DG/DT SAME AS ABOVE SEARCH FOR DV/DT = 0.0. IF DG/DT = 0.0
C AT ALPHA = ALPHMX, PROGRAM FAILS. ALPHA2 IS REQUIRED VALUE OF ALPHA
C FOR DG/DT = 0.0.
C
106 ALPXUP = ALPHMX
110 YUP = DGDT(ALPXUP)
112 IF (YUP .LT. 0.0) GO TO 99
120 5 ALPXLO = ALPXUP - 2.0
122 IF (ALPXLO .LT. ALPHMX) GO TO 7
125 YLO = DGDT(ALPXLO)
126 IF (YLO * YUP .LE. 0.0) GO TO 6
134 ALPXUP = ALPXLO
135 YUP = YLO
137 GO TO 5
137 6 ALPHA2 = ZEROX(ALPXLO,ALPXUP,DGDT,EPS)
C
C FIND ERROR BETWEEN ALPHA1 AND ALPHA2.
C
142 ERROR = (ALPHA1 - ALPHA2) / ALPHMX
145 IF (ABS(ERROR) .LT. 0.005) GO TO 10
154 IF (ABS(ERROR) .LT. 0.01) .AND. JC .GT. 25) GO TO 10
165 IF (JX .EQ. 2) GO TO 10
C
C MAKE NEW GUESS AT THRUST AND REPEAT DV/DT AND DG/DT LOOPS UNTIL
C ALPHA1 = ALPHA2 (WITHIN TOLERANCES).
C
167 CALL ITRJVB(ERROR,ERRM1,THRUST,TOL,JC,JX)
175 IF (JC .GT. 30) GO TO 99
204 GO TO 2
204 10 ALPHA = ALPHA1
206 RETURN
206 98 NER = 9
207 WRITE(6,101) THRUST,ALPHA,ERRM1,ERRM2,ERRM1,JC
101 FORMAT(10X,10H*** FAILED IN ZERO,15X,51HNO SOLUTION FOR DVDT -TH
9RUST,ALPHA,ERROR,ERRM1,JC =,2F9.2,2F7.4,13)
RETURN
231

```

```

ZERO      231      99 NER = 9
          232      WRITE (6,100) TFIRST, YUP, ERROR, ERRM1, ALPHA1, ALPHA2, JC
          100 FORMAT (/, 2X, 10H*** FAILED IN ZERO,/, 5X, 42H TFIRST,YUP,ERROR,ERR
          0M1,ALPHA1,ALPHA2,JC = , 6F12.4, 14)
          260      RETURN
          260      END

```

SUBPROGRAM LENGTH

00365/01

FUNCTION ASSIGNMENTS

STATEMENT	ASSIGNMENTS	1	2	3	4	5	6
1	- 000021	10	- 000040	98	- 000065	99	- 000104
7	- 000060	10	- 000205	98	- 000207	100	- 000313
							101

BLOCK NAMES AND LENGTHS

UNIV - 000030/01 AERO - 000020/02 LAND - 000003/03

VARIABLE ASSIGNMENTS

VARIABLE	ASSIGNMENTS	ALPHA	ALPHA1	ALPHA2	ALPHA3	ALPHMN	ALPHMX	ALPHXLO
ALPHA	- 000010/02	BL	- 000361	BU	- 000364	EM	- 000002/03	EPS
ALPHXUP	- 000355	BL	- 000350	F	- 000347	JC	- 000021/01	EPS
ERRM1	- 000354	ERROR	- 000353	THRUST	- 000345	JC	- 000352	QUEST
ST	- 000004/01	TFIRST	- 000344	YLO	- 000003/02	TOL	- 000006/01	WF
XLO	- 000360	XUP	- 000356	YLO	- 000363	YUP	- 000007/01	

START OF CONSTANTS-000263 TEMPS--000326 INDIRECTS-000342

7600 COMPILATION -- RUN76 LEVEL 5C 73/07/04.

ROUTINE COMPILES IN 044600

DVDT

```

C
C FUNCTION SUBROUTINE DVDT COMPUTES DV/DT AS A FUNCTION OF ALPHA.
C REQUIRES VARIABLES W,OS,CX,GAMAPP
C
COMMON /UNIV/ NPC ,NSC ,IDC ,H ,R ,W ,
1WF ,EM ,VMO ,ENHO ,ALPHL0,CLAL ,AR ,B ,
2EVEW ,EMP ,TA ,WG ,WGS ,KWP ,
3,XSIZE
COMMON /AERO/ VEL,OS,MABS,THRUST,TVECT,DEL,E,DELF,DELSPL,ALPHA,
9CX,CY,CL,CD,RHO,GRCD,IFAST
COMMON/LAND/ GAMAPP,VKAPP,ALPHAX
GAMX = -GAMAPP * .0174533
ALPHA = ALPHAX
CALL ARGOYN
DVDT = (12.2 / W) * (-CX * OS - W*SIN(GAMX))
15 RETURN
16 END

```

SUBPROGRAM LENGTH

00036

FUNCTION ASSIGNMENTS

STATEMENT ASSIGNMENTS

BLOCK NAMES AND LENGTHS

(NIV - 000030/0) AERO - 000020/02 LAND - 000003/03

VARIABLE ASSIGNMENTS

ALPHA - 000010/02 CX

W - 000006/01

START OF CONSTANTS-000021

TEMPS--000024

INDIRECTS-000034

7600 COMPILATION -- RUN76 LEVEL 5C 73/07/04.

ROUTINE COMPILES IN 044000

- 000001/02

OS

- 000035

GAMX

GAMAPP - 000000/03

```

DGDY      FUNCTION DGDY(ALPHA)
C
C  FUNCTION SUBROUTINE DGDY COMPUTES DG/DY AS A FUNCTION OF ALPHA.
C  REQUIRES VARIABLES W,OS,VEL,CY,GAMMA
C
COMMON /UNIV/ NPC, NSC, IDC, H, ST, R, W,
/ME/ EM, VMO, EMMD, ALPHLO, CLALPH, SW, AR, B,
ZEYEW, ENP, TA, WG, WGS, KWRITE, DLMC4
3,KSIZE
COMMON /AERO/ VEL,OS,HABS,THRUST,TVECT, ANGLE,DELFD,DELSPL,ALPHA,
9CX,CY,CL,CD,RHO,GRCD,IFAST
COMMON/LAND/ GAMMA,VKAPP,ALPHMX
GAMX = -GAMMA * .0174533
ALPHA = ALPHAY
CALL ARDYN
DGDY = (32.2 / (W*VEL)) * (CY * OS - W * COS(GAMMA))
RETURN
END
4
5
6
16
17

SUBPROGRAM LENGTH
00041

FUNCTION ASSIGNMENTS
STATEMENT ASSIGNMENTS
BLOCK NAMES AND LENGTHS
UNIV - 000030/01 AERO - 000020/02 LAND - 000003/03
VARIABLE ASSIGNMENTS
ALPHA - 000010/02 CY - 000012/02 DGDY - 000037 GAMMA - 000000/03
VEL - 000000/02 W - 000006/01
START OF CONSTANTS--000022 TEMPS--000025 INDIRECTS--000037
7600 COMPILATION -- RUN76 LEVEL 5C 73/07/04.
ROUTINE COMPILES IN 044000
OS - 000001/02

```